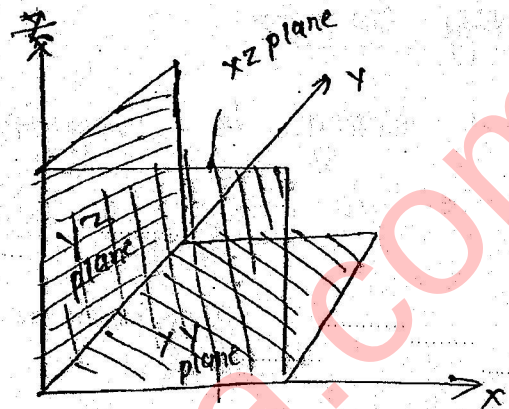


3-D Space co-ordinate system $\Rightarrow$

Angular velocity ($\vec{\omega}$)

Vector quantity

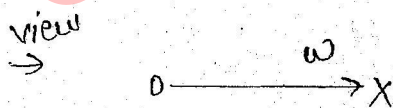
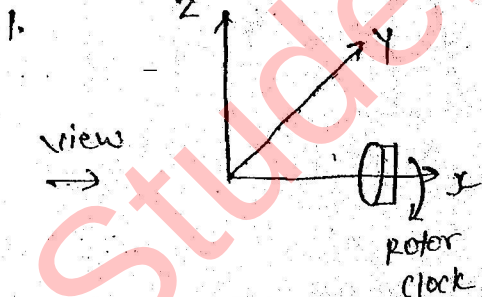
Mag. $\rightarrow$ rate of change of Angular Displacement
 Dirⁿ $\rightarrow$ Predicted by Right Hand thumb rule.



Dirⁿ of ω also known as Axis of spin

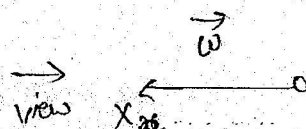
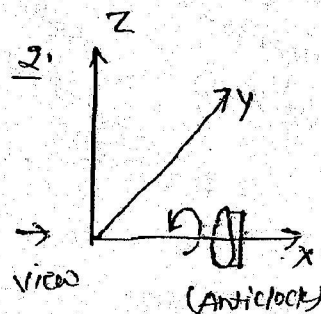
- 1 $\rightarrow$ Place right hand in such a way that fingers are $\perp$ to the thumb.
- 2 $\rightarrow$ Rotate the fingers in the sense of rotation, then the dirⁿ of thumb will be the dirⁿ of Angular velocity.

For Exq $\Rightarrow$



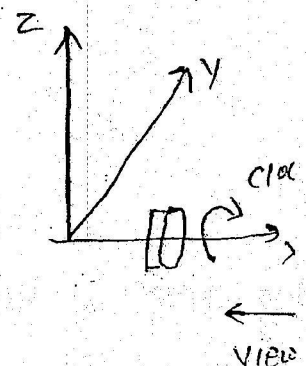
Axis of spin $\rightarrow$ OX

plane of spin $\rightarrow$ YZ



Axis of spin $\rightarrow$ OX

plane of spin $\rightarrow$ YZ



Axis of spin $\rightarrow$ OX

plane of spin $\rightarrow$ YZ

Angular Accⁿ (α) $\Rightarrow$

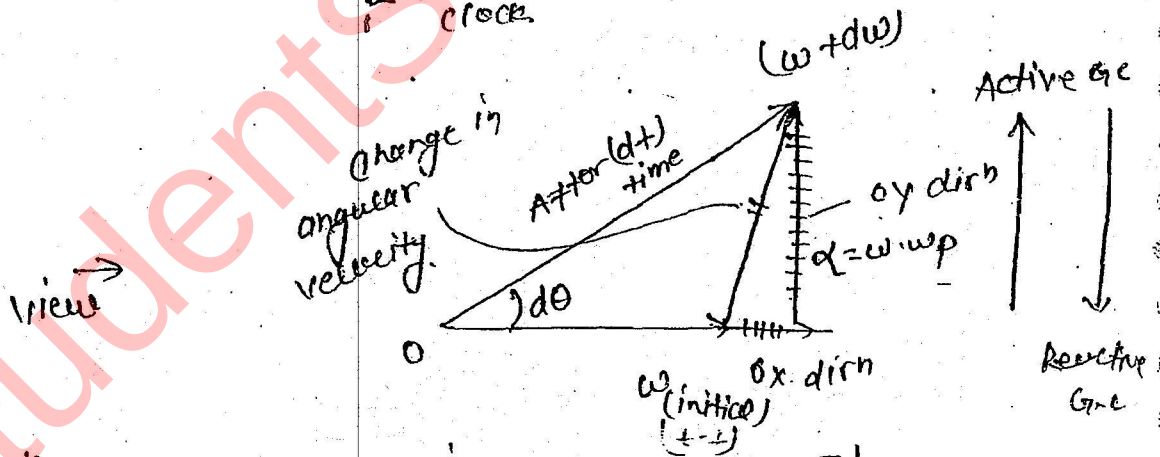
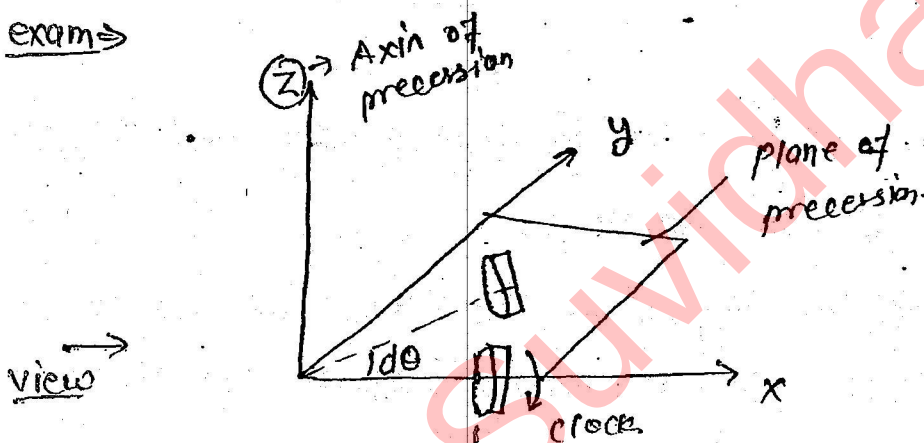
$$\vec{\alpha} = \frac{d\vec{\omega}}{dt}$$

α may come $\Rightarrow$

- Due to change in magnitude of $\vec{\omega}$.
- Due to the change in Dirⁿ of $\vec{\omega}$.

Phenomenon $\rightarrow$ (precession)

for exam $\Rightarrow$



Ang. Accⁿ because of change in magnitude of $\vec{\omega}$

$$\Rightarrow \frac{(\omega + d\omega) \cos d\theta - \omega}{dt}$$

$$\Rightarrow \frac{(\omega + d\omega) - \omega}{dt}$$

$$\Rightarrow \left(\frac{d\omega}{dt} \right) \text{ (ox dirⁿ)}$$

Angular Acceleration

because of the change in dirⁿ of $\vec{\omega}$ $\Rightarrow \frac{(\omega + d\omega) \sin \theta - 0}{dt} = \frac{(\omega + d\omega) d\theta}{dt}$

$$\Rightarrow \frac{\omega \cdot d\theta + \cancel{d\omega \cdot d\theta}}{dt} = \omega \cdot \left(\frac{d\theta}{dt} \right) = \omega \cdot \omega_p \quad (\text{or dir}^n)$$

$\omega_p \Rightarrow$ Ang. velocity of precession

$$(\omega_p = \frac{d\theta}{dt})$$

Total ang. Accelⁿ

$$\vec{\alpha} = \left(\frac{d\omega}{dt} \right) \hat{i} + (\omega \cdot \omega_p) \hat{j}$$

$\Downarrow$
Gyroscopic Accelⁿ

If only dirⁿ of $\vec{\omega}$ is changing, magnitude is not changing

Then $\alpha = (\omega \cdot \omega_p) \quad (\text{or dir}^n)$
 $\Downarrow$
Gyroscopic Accelⁿ.

Therefore to have a precession (ie to change the dirⁿ of $\vec{\omega}$)

In order to provide the $\alpha = \omega \cdot \omega_p$ (or dirⁿ),

An external torque is required to be applied to the sys

$\Downarrow$

That external requirement of torque is known as

Action Gyroscopic couple.

Then!

$$\alpha = (\omega \cdot \omega_p) \text{ (oy dir)} \downarrow$$

Gyroscopic
Acceleration

$$C = I \alpha$$

$$C = I \omega \cdot \omega_p \text{ (oy dir)}$$

Similar torque will be applied by the system to the external agency in reverse dir.

and that torque is known as reactive gyroscopic couple

$$C = I \omega \cdot \omega_p \text{ (oy dir)}$$

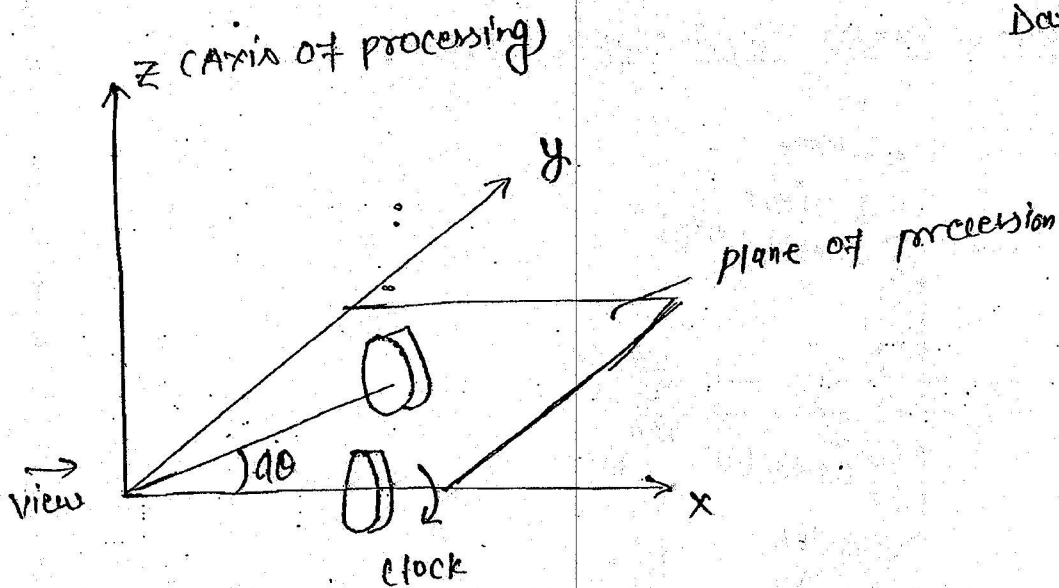
And this torque will also be experienced by the system itself because that external agency is the part of system.

After effect of gyroscopic action on the system

$\downarrow$

Reactive Gyroscopic couple

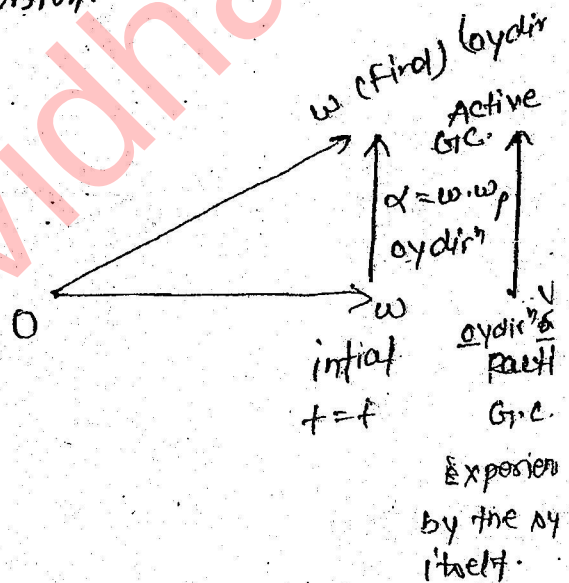
Date - 17/Jun/201



$\omega \rightarrow$ Ang. velocity of rotor.

$\omega_p \rightarrow$ Ang. velocity of precession.

$$\omega_p = \frac{d\theta}{dt}$$



OX - Axis of spin

YZ - plane of spin

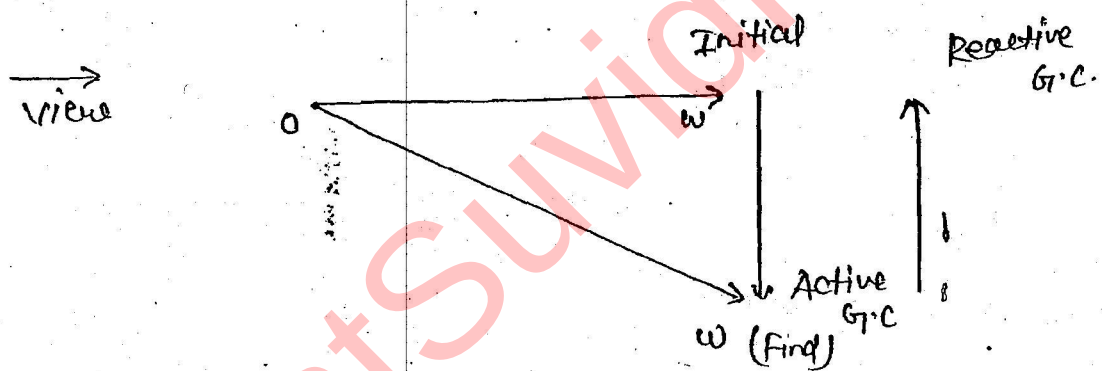
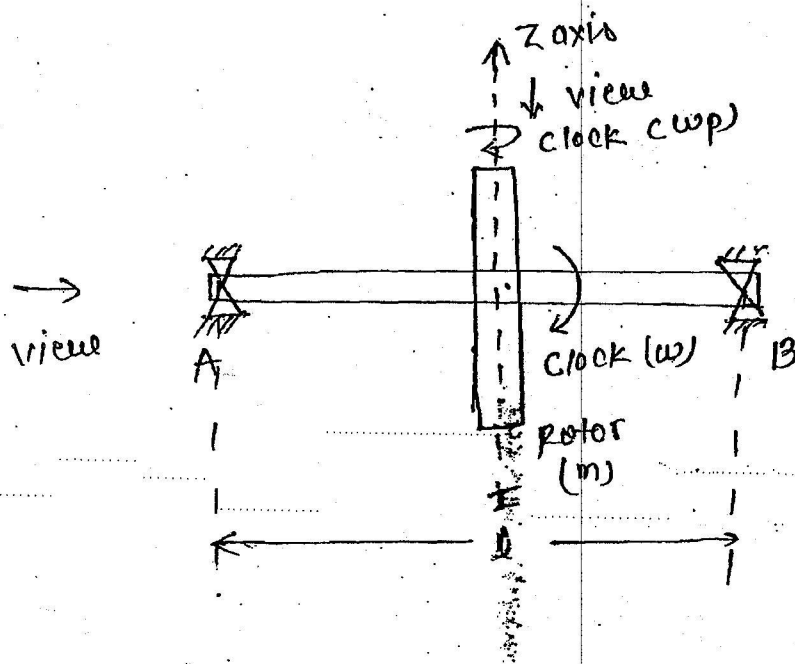
OZ - Axis of precession

XY - plane of precession

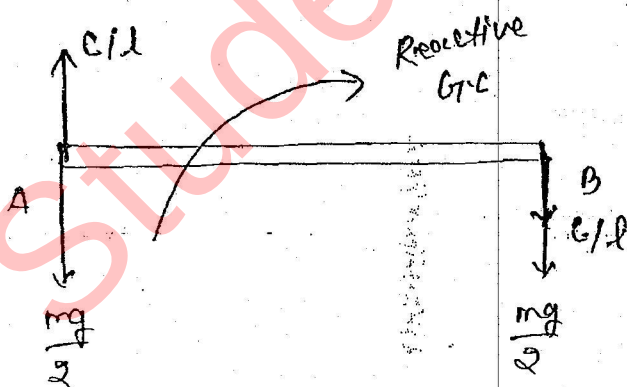
OY - Axis of gyroscopic couple

XZ - plane of gyroscopic couple.

Bearings · Reactions under Gyroscopic effect



Force on shaft



Bearing Reaction Rxn

$$R_A = \left(\frac{c}{l} - \frac{mg}{2} \right) \text{ (downward)}$$

$$R_B = \left(\frac{c}{l} + \frac{mg}{2} \right) \text{ (upward)}$$

$$F_A = \left(\frac{c}{l} - \frac{mg}{2} \right) \text{ (upward)}$$

$$F_B = \left(\frac{c}{l} + \frac{mg}{2} \right) \text{ (downward)}$$

Q4 ≥ 16

$$d = 0.2 \text{ m}$$

$$r = 0.1 \text{ m}$$

$$m = 10 \text{ kg}$$

$$I = \frac{mr^2}{2} \text{ (known)}$$

$$l = 0.150 \text{ m}$$

$$N = 2000 \text{ rpm}$$

$$\omega = \frac{2\pi N}{60} \text{ rad/s}$$

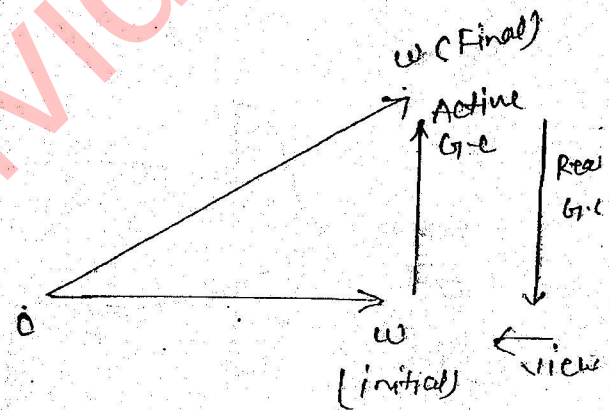
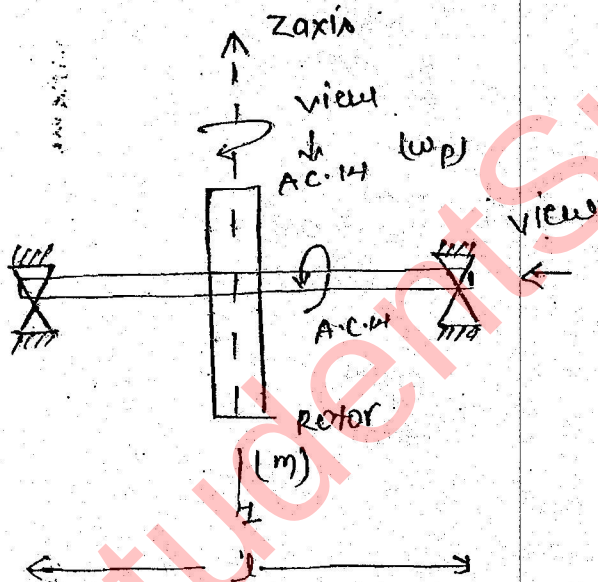
$$N_p = 50 \text{ rpm}$$

$$\omega_p = \frac{2\pi \times 50}{60}$$

$$C = I \cdot \omega \cdot \omega_p = 54.8103 \text{ N-m}$$

$$\frac{C}{l} = \frac{54.8103}{0.150} = 365.4553 \text{ N}$$

$$mg = 10 \times 9.81 = 98.1 \text{ N}$$



Force on shaft

$$F_B = \left(\frac{C}{l} - \frac{mg}{2} \right) \text{ upward}$$

$$F_A = \left(\frac{C}{l} + \frac{mg}{2} \right) \text{ downward}$$



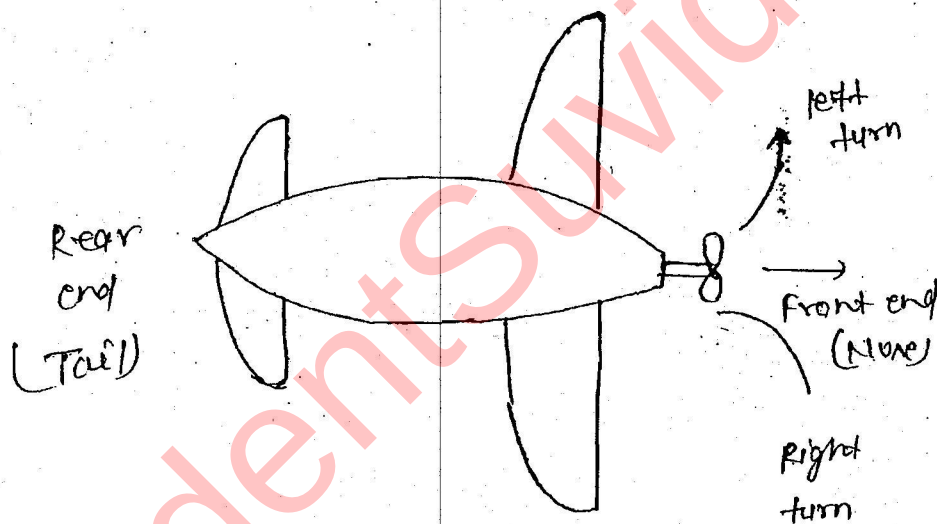
Bearing Reaction

$$R_B = \left(C/l - \frac{mg}{2} \right) \quad (\text{downward})$$

$$R_A = \left(C/l + \frac{mg}{2} \right) \quad (\text{upward}) = 414$$

Gyroscopic effect on turning of Aircraft $\Rightarrow$

Front end of the aircraft is known as Nose and the Rear end of the aircraft is known as Tail.



$$(\omega_p)_{\text{Turning}} = \frac{V}{R}$$

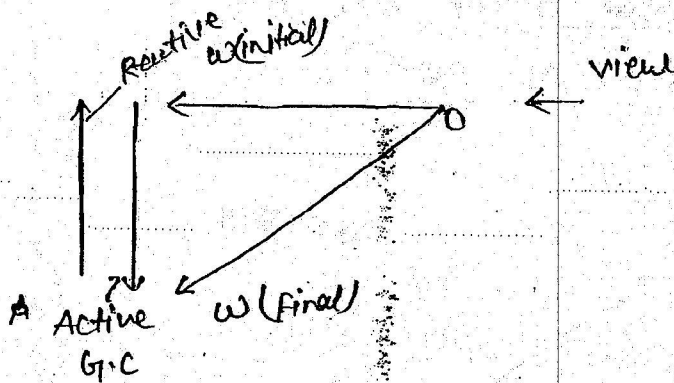
$V \rightarrow$ velocity of turn

$R \rightarrow$ Radii of Turn.

viewed from nose (from end)

(Engine rotates clockwise)

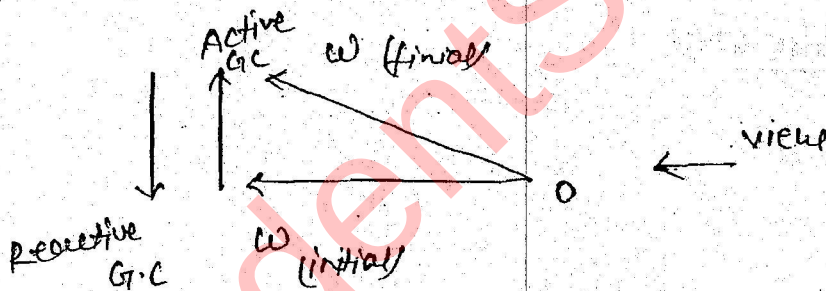
1- Left turn



Effect

Nose will go down & Tail will go up.

2- Right turn $\Rightarrow$



Effect $\Rightarrow$

Nose will go up & Tail will go down.

Gyroscopic effect on ship during turning

Front end of the ship is known as Bow and the Rear end of the ship is known as Stern.

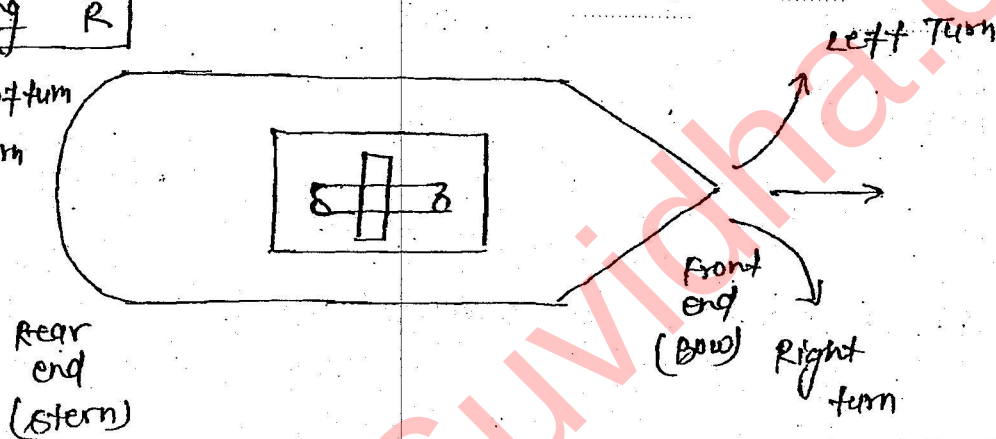
Looking from ~~stern~~ stern side the R.H.S of the ship portion is known as Star Board and the L.H.S portion of ship is known as port.

$$(\omega_p)_{\text{turning}} = \frac{v}{R}$$

$v \rightarrow$ velocity of turn

$R \rightarrow$ radi of turn

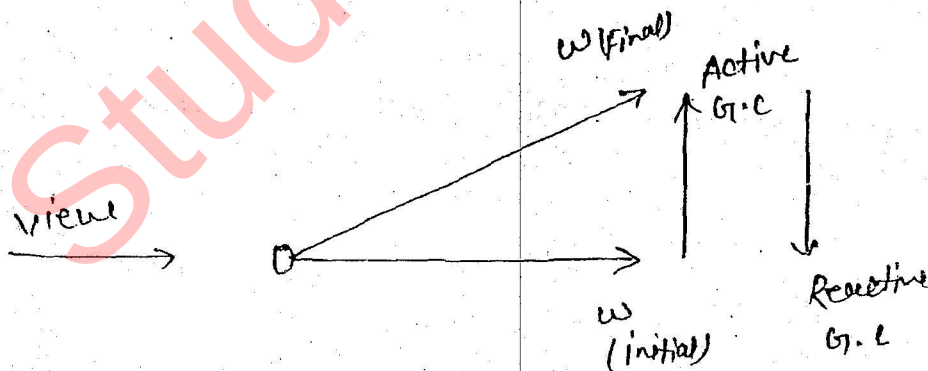
$\rightarrow$ view



viewed from stern (Rear End)

Engine Rotate clockwise

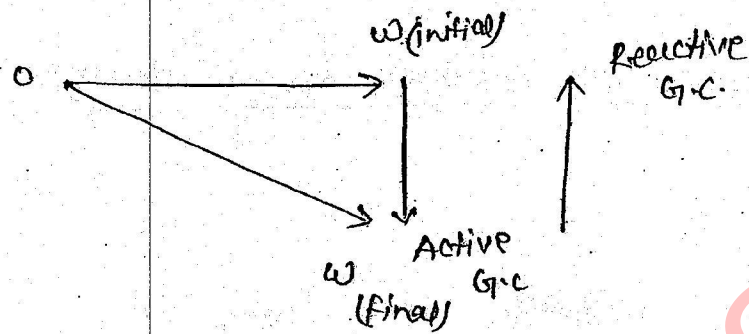
① Left turn



Effect $\rightarrow$ Bow will go up and stern will go down.

② Right turns

view
→

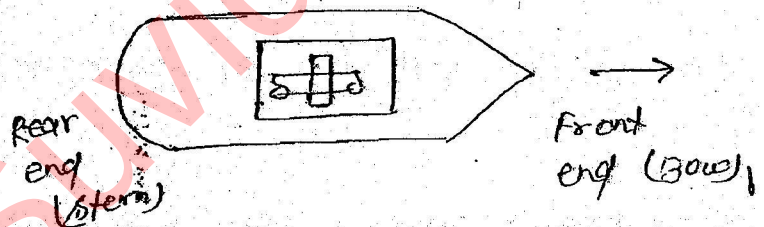


Effect $\Rightarrow$ Bow will go down & stern will go up.

Gyroscopic effect on ships during pitching $\Rightarrow$

$\omega \rightarrow$ speed of engine

$\omega_p \rightarrow$ For pitching
↓
oscillation



If $T \rightarrow$ Time period of oscillation of pitching.

$$(\omega_p)_{\text{pitching}} = \frac{2\pi}{T}$$

Transverse axis - pitching
longitudinal axis - Rolling

$$x = A \sin \omega_n t$$

$$\theta = \theta_0 \sin \omega_n t$$

$$\omega_p = \frac{d\theta}{dt} = (\theta_0 \cdot \omega_n) \cdot \cos(\omega_n t)$$

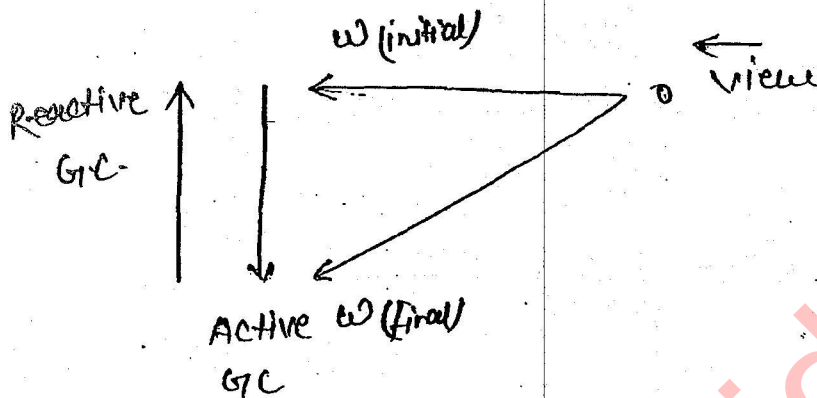
$$(\omega_p)_{\text{max}} \text{ (pitching)} = \theta_0 \cdot \omega_n \text{ (rad)}$$

Angular
Amplitude.

viewed from Bow! $\Rightarrow$

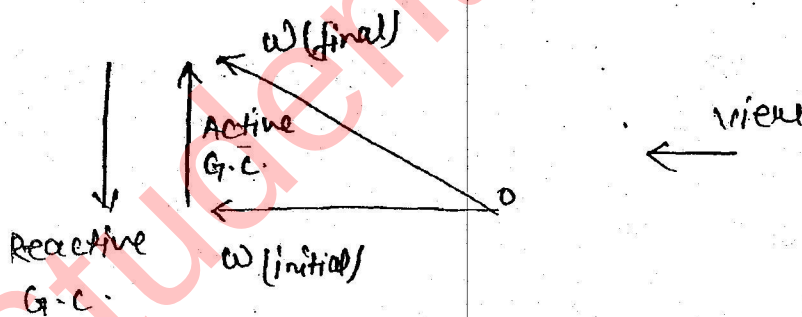
Engine rotate clockwise

1 $\rightarrow$ Bow moves up (stern moves down)



Effect $\Rightarrow$ Ship will try to turn towards left (port) side.

2 $\rightarrow$ Bow moves down (stern moves up)



Effect $\Rightarrow$ Ship will try to turn towards right (star board side)

Gyroscopic effect on ships under rolling $\Rightarrow$

During rolling, The direction of Angular velocity is not changing

$$\Rightarrow \omega_p = 0$$

$$\Rightarrow I \cdot \omega \cdot \omega_p = 0$$

Ship will not experience any Gyroscopic effect during Rolling.

Effect (Gyroscopic) on a 4-wheeler during Turning $\Rightarrow$

$I_E \rightarrow$ M.I. of Engine.

$I_W \rightarrow$ M.I. of wheel.

$\omega_E \rightarrow$ speed of engine

$\omega_W \rightarrow$ speed of wheel

$\omega_p \rightarrow \frac{V}{R}$ (Turning)

$\rightarrow$ same for wheel and engine.

Gyroscopic couple $\Rightarrow$

Engine $C_E = I_E \cdot \omega_E \cdot \omega_p$

Wheel: $C_W = 4 \cdot I_W \cdot \omega_W \cdot \omega_p$

Total Gy. Couple

$$C = C_E \pm C_W$$

$$C = (I_E \cdot \omega_E \pm 4 I_W \cdot \omega_W) \cdot \omega_p$$

If $l \rightarrow$ distance b/w inner and outer wheel.

for each on wheel

For on each Inner wheel ~~2 outer wheels~~ $= \frac{C}{2l}$ (up word)

Force on each outer wheel $= \frac{C}{2l}$ (downward)

Gy. effect during Turning.

Pb-17

Solve

$$m = 3500 \text{ kg}$$

$$k = 0.45 \text{ m}$$

$$I = mk^2$$

$$I = 708.75 \text{ kg-m}^2$$

$$N = 3000 \text{ rpm}$$

$$\omega = \frac{2\pi \times 3000}{60}$$

$$\omega = 100\pi = 314.15922 \text{ rad/s}$$

④

$$(\omega_p)_{\text{Turning}} = \frac{v}{R} = \frac{(36 \times \frac{5}{18})}{100} = 0.1 \text{ rad/s}$$

$$C = I \cdot \omega \cdot (\omega_p)_{\text{Turning}}$$

$$= 22266.033 \text{ N-m}$$

$$\textcircled{b} \quad \omega_n = \frac{2\pi}{T} = \frac{2\pi}{40} = 0.157 \text{ rad/s.}$$

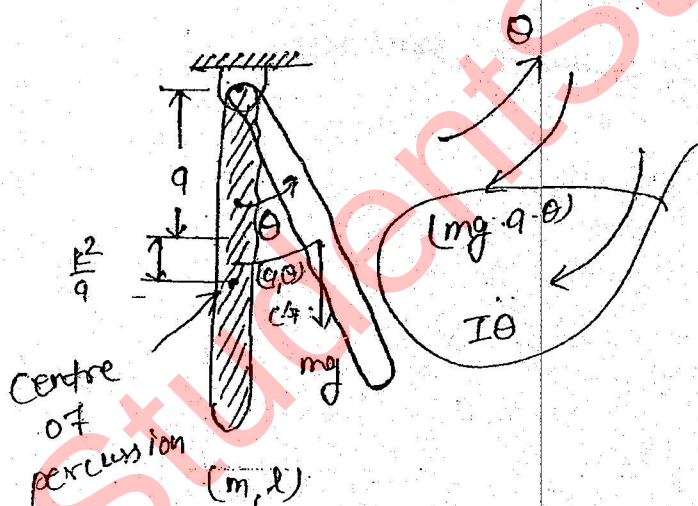
$$\theta_0 = 6^\circ = \frac{6\pi}{180} = \frac{\pi}{30} \text{ rad}$$

$$\begin{aligned} (\omega_p)_{\text{pitching}} &= \theta_0 \cdot \omega_n \\ &= \frac{\pi}{30} \times 0.157 \\ &= 0.01644 \text{ rad/s.} \end{aligned}$$

$$\begin{aligned} C &= I \cdot \omega \cdot (\omega_p)_{\text{pitching}} \\ &= 3659.0468 \text{ N-m} // \end{aligned}$$

Date 10/Jun/2016

Compound pendulum $\Rightarrow$



k = Radius of Gyration

(About CG Axis)

$$I\ddot{\theta} + (mg \cdot q) \theta = 0$$

$$(\frac{1}{2}k^2 + \frac{1}{2}l^2) \ddot{\theta} + \frac{1}{2}mg \cdot q \cdot \theta = 0$$

$$\ddot{\theta} + \left(\frac{g}{\frac{k^2 + l^2}{2}} \right) \theta = 0$$

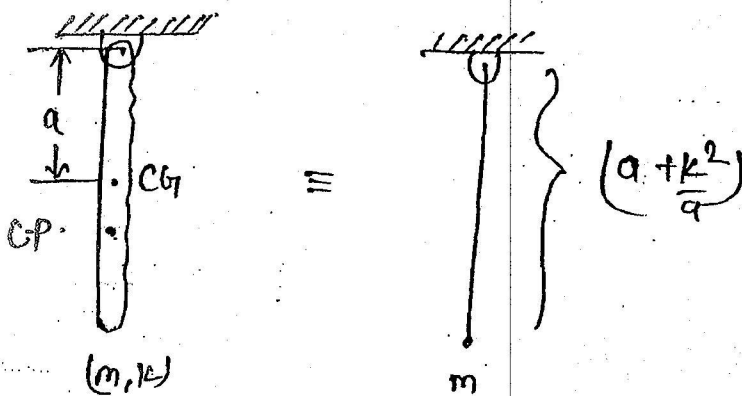
$$\ddot{\theta} + \left(\frac{g}{\left(q + \frac{k^2}{q} \right)} \right) \theta = 0$$

$$\omega_n = \sqrt{\frac{g}{\left(q + \frac{k^2}{q} \right)}}$$

$$T = 2\pi \sqrt{\frac{q + \frac{k^2}{q}}{g}} = 2\pi \sqrt{\frac{le}{g}}$$

Here -

$$I_c = \left(a + \frac{k^2}{a} \right)$$

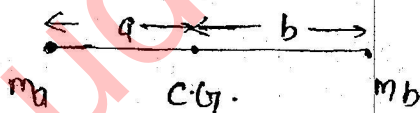
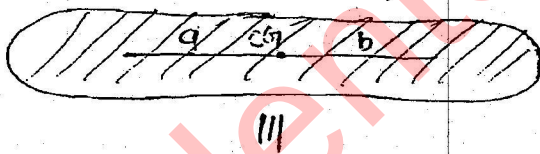


Dynamically equivalent system $\Rightarrow$

The system is going to be said as dynamically equivalent if.

- 1) Total mass of the system is same.
- 2) Centre of gravity must be same.
- 3) Moment of inertia must be same.

Body cm. $\rightarrow$ Rad. of Gyration about C.G.



$$m_a + m_b = m \quad \text{--- (1)}$$

$$m_a \cdot a = m_b \cdot b \quad \text{--- (2)}$$

$$m_a \cdot a^2 + m_b \cdot b^2 = m \cdot k^2 \quad \text{--- (3)}$$

By eqn ① & ②

$$m_a + m_b \cdot \frac{a}{b} = m$$

$$m_a \cdot \frac{(a+b)}{b} = m$$

$$m_a = \frac{m \cdot b}{(a+b)}$$

$$m_b = \frac{m \cdot a}{(a+b)}$$

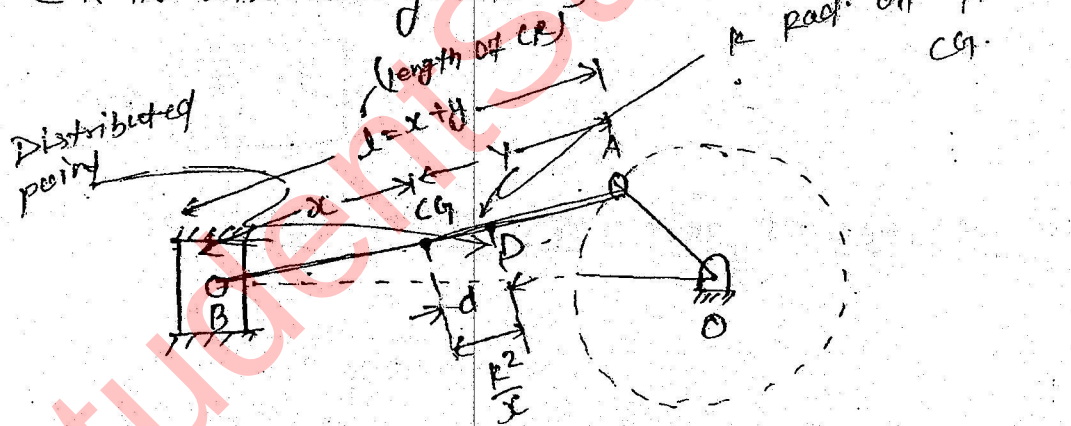
$$\frac{m \cdot b}{(a+b)} \cdot a^2 + \frac{m \cdot a}{(a+b)} \cdot b^2 = m k^2$$

$$a b \frac{(a+b)}{(a+b)} = k^2$$

$$[k^2 = ab] \quad b = \frac{k^2}{a}$$

Correcting couple (Torque)

(C.R. is also having Inertia)



For C.R. to be

Dynamically equivalent system mass must be distributed at B & D

But in the analysis it is convenient to distribute the mass of CR and B & A instead of B & D.

Therefore there is a correction in Torque,

Correcting Torque (ΔT)

$$m = I/d^2 = m k^2/d$$

$$\Delta T = \frac{m \cdot d_c (x \cdot y)}{\text{we are taking this}} - \frac{m d_c (x \cdot d)}{\text{Actual}}$$

$$= m d_c \cdot x [y - d]$$

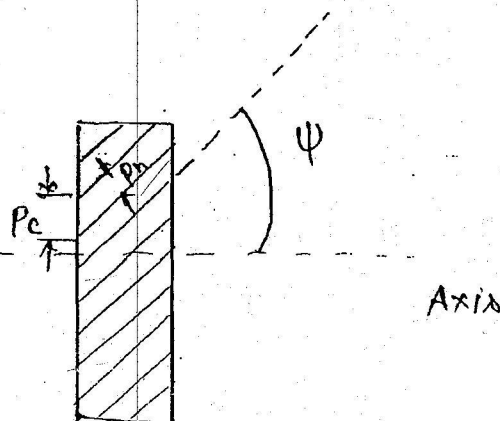
$$= m d_c \cdot x [(x+y) - (x+d)]$$

$$\Delta T = m d_c \cdot x [L - L]$$

$$L = x + d$$

$$d = \frac{k^2}{x}$$

Terminology of Helical gear or spiral gear $\Rightarrow$



ψ = spiral angle (Helix angle)

P_c = circular pitch

P_n = Normal pitch

$$P_n = P_c \cos \psi$$

For two mating Gears :-

$$* P_{n1} = P_{n2}$$

$$P_c = \pi \cdot m$$

$$P_n = \pi \cdot m_n$$

$$m_n = m \cdot \cos \psi$$

For two mating Gear -

$$m_{n1} = m_{n2}$$

$\theta \rightarrow$ Angle b/w two shaft

1 $\rightarrow$ Driver

2 $\rightarrow$ Driven

$\theta = (\psi_1 + \psi_2)$ (same Handed Gears)

$\theta = (\psi_1 - \psi_2)$ (opposite Handed Gears)

Note:- If in the problem, it is not given that which hand gear in contact then always take same hand.

$$* \theta = \psi_1 + \psi_2$$

Centre distance $\geq$

$$\begin{aligned} & r_1 + r_2 \\ &= \frac{m_1 T_1}{2} + \frac{m_2 T_2}{2} \end{aligned}$$

$$= \frac{m_1}{\cos \psi_1} \cdot \frac{T_1}{2} + \frac{m_2}{\cos \psi_2} \cdot \frac{T_2}{2}$$

$$= \frac{m_1}{2} \left[\frac{T_1}{\cos \psi_1} + \frac{T_2}{\cos \psi_2} \right]$$

velocity ratio (V.R) $\Rightarrow$

$$V_{\text{normal}} = V_1 \cos \psi_1 = V_2 \cos \psi_2$$

$$\frac{V_2}{V_1} = \frac{\cos \psi_1}{\cos \psi_2}$$

$$V.R = \frac{\omega_2}{\omega_1} = \frac{V_2}{\frac{r_2}{r_1}} = \frac{V_2}{V_1} \cdot \frac{r_1}{r_2}$$

$$\begin{aligned} V.R &= \frac{V_2}{V_1} \cdot \frac{\frac{m_1 T_1}{2}}{\frac{m_2 T_2}{2}} \\ &= \frac{V_2}{V_1} \cdot \frac{m_1}{m_2} \cdot \frac{T_1}{T_2} \\ &= \frac{V_2}{V_1} \cdot \frac{\frac{m_1}{\cos \psi_1}}{\frac{m_2}{\cos \psi_2}} \cdot \frac{T_1}{T_2} \end{aligned}$$

$$= \frac{\cos \psi_1}{\cos \psi_2} \cdot \frac{\cos \psi_2}{\cos \psi_1} \cdot \frac{T_1}{T_2}$$

$$V.R = \frac{T_1}{T_2}$$

Efficiency $\Rightarrow$

$$\eta = \frac{F_2 \cdot V_2}{F_1 \cdot V_1}$$

$$\eta = \frac{\cos(\psi_2 + \phi)}{\cos(\psi_1 - \phi)} \cdot \frac{\cos \psi_1}{\cos \psi_2}$$

ϕ = pressure angle

if μ = coefficient of friction

$$\phi = \tan^{-1} \mu$$

Max efficiency

$$\eta_{\max} = \frac{1 + \cos(\theta + \phi)}{1 + \cos(\theta - \phi)}$$

$$\theta = \psi_1 + \psi_2$$

$$\psi_1 = \frac{(\theta + \phi)}{2}$$

Terminology of Worm wheel $\Rightarrow$

- 1- WORM
- 2- Worm wheel

$$\theta = 90^\circ$$

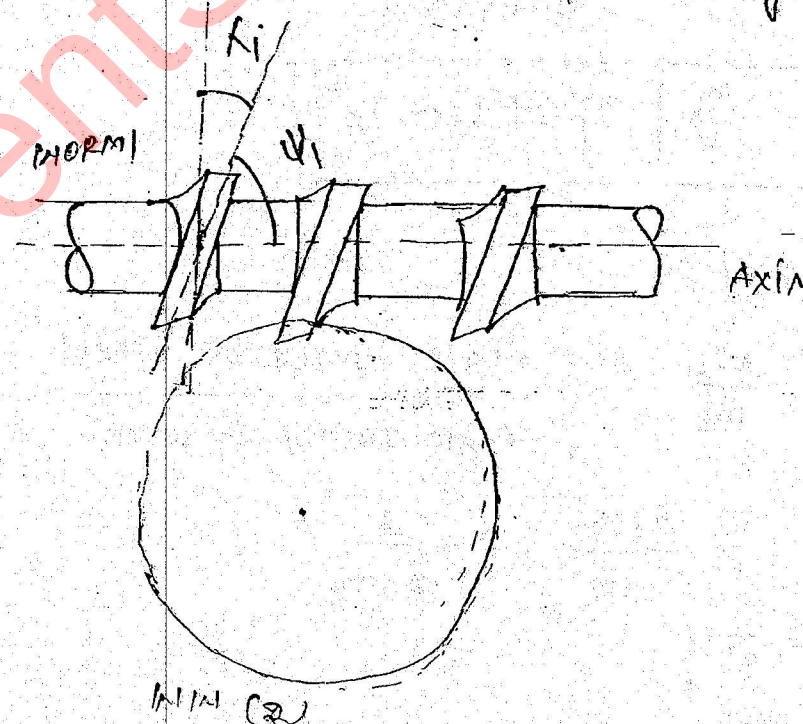
$$\lambda_1 + \psi_1 = 90^\circ$$

$$\psi_1 = (90^\circ - \lambda_1) \quad *$$

$$\theta = \psi_1 + \psi_2$$

$$90^\circ = (90^\circ - \lambda_1) + \psi_2$$

$$\psi_2 = \lambda_1 \quad *$$



λ_1 = lead angle

$$\tan \lambda_1 = \frac{\text{lead}}{\pi d_1}$$

$$\boxed{\tan \lambda_1 = \frac{l}{\pi d_1}}$$

$$l = \text{lead} = p \text{ (single start)}$$

$$= 2p \text{ (Double start)}$$

$$= 3p \text{ (Triple start)}$$

Centre distance $\Rightarrow$

$$= \frac{m_h}{2} \left[\frac{T_1}{\cos \psi_1} + \frac{T_2}{\cos \psi_2} \right]$$

$$= \frac{m_2 \cos \psi_2}{2} \cdot \frac{1}{\cos \psi_2} \left[\frac{T_1 \cos \psi_2}{\cos \psi_1} + T_2 \right]$$

$$= \frac{m_2}{2} \left[\frac{T_1 \cos \lambda_1}{\cos (90^\circ - \lambda_1)} + T_2 \right]$$

$$\boxed{= \frac{m_2}{2} [T_1 \cot \lambda_1 + T_2]}$$

Velocity Ratio $\Rightarrow$

$$VR = \frac{\omega_2}{\omega_1} = \frac{\text{Angle turned by wheel}}{\text{Angle turned by worm}}$$

$$= \frac{l/r_2}{2\pi} = \frac{l}{2\pi r_2}$$

$$\boxed{VR = \frac{l}{\pi d_2}}$$

Efficiency (η)

$$\eta = \frac{\cos(\lambda_1 + \phi)}{\cos(90^\circ - (\lambda_1 + \phi))} \cdot \frac{\cos(90^\circ - \lambda_1)}{\cos \lambda_1}$$

$$\eta = \frac{\tan \lambda_1}{\tan(\lambda_1 + \phi)}$$

$$\eta_{\max} = \frac{1 - \sin \phi}{1 + \sin \phi}$$

