Essor analysis steady state error It is a measure of system accurac It is the diff. b/w i/p & o/p of the su during steady state for accuracy steady state our should be nin. C(S) $R(s) = (x) \frac{E(s)}{x}$ 60 C(S) = G(S)R(s) = 1 + G(s) H(s)1----- $C(s) = E(s) \cdot O(s)$ $\frac{E(s)}{R(s)} = \frac{1}{1 + G(s) + (s)}$ E(S) = steady state = R(S) 1+G(S)H(S) error final value theorem can be used to find steady state error Eq o for unity feedback $e_{SS} = \lim_{t \to \infty} e(t) = \lim_{s \to 0} SE(s) - \lim_{s \to 0} SE(s)$

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$$\frac{1}{1+\frac{1}{2}}$$
Static velocity error constant (Kp)

$$\frac{1}{1+\frac{1}{2}}$$

$$\frac{1}{1+\frac{$$

1

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Static accelaration error constant $R(S) = \frac{1}{\Delta^3}$ $e_{ss} = l + \underline{AR(s)}$ $\underline{A \rightarrow 0} \quad \bullet 1 + G(s) H(s)$ $e_{ss} = \underbrace{lt}_{\Delta \to 0} \underbrace{1}_{\Delta^2 + \Delta^2 G(S) H(S)}$ 0+12F 5 G(S) H(S) ess = 1 $K_q = Qt \Delta^2 G(S) HI$ Ka * open loop to ansfer fut. $G_1(S) = K(1+ST_1) \circ (1+ST_2)$ $S^m (1+ST_a) (1+ST_b)$ m determines type of system m = 0 Type '0' Cantrof system Type (1))) Type (2) 2 1) Essor analysis in diff. Types of systems Type O Type 1 Type 2 × OYK 00 IFK 00 VK 00 System type is defined as the no of put integrator in a system.

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classmate A BOTYPE O unit step R(S) → 1 $G(S) H(S) = \frac{K(1+ST_1)(1+ST_2)}{(1+ST_3)(1+ST_6)} =$ forr unit step CAN = 1 I+KP Kp = lt G(s) H(s) A⇒0 $K\rho = Q + K(1+sT_0)(1+sT_2)$ $A^{30} (1+sT_q)(1+sT_b)$ Kp = KEAS = 1 Itk R(s) = 1 $K_{\gamma} = \begin{smallmatrix} H & \Delta G_{\gamma}(S) & H(S) \\ \Delta S_{\gamma}(S) & H(S) \end{smallmatrix}$ KV= 0 $e_{XX} = 1 = 1 = \infty$ $K_V = 0$ A Type O appelle parabolic $\mathbf{R}(s) = 1$ $K_q = l + s^2 G(s) H(s) \qquad e_{ss} = \frac{1}{Kq}$ $V_s = 0$ $E_{ss} = 0$

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Type 1 unit step R(S) = J\$X $F^{e}_{G_{1}(S)} H(S) = K(1+ST_{1})(1+ST_{2}) - S(1+ST_{a})(1+ST_{b}) - S(1+ST_{a})(1+ST_{b}) - S(1+ST_{a})(1+ST_{b}) - S(1+ST_{a})(1+ST_{b}) - S(1+ST_{a})(1+ST_{b}) - S(1+ST_{b})(1+ST_{b}) - S(1+ST_{b})(1+ST_{b})(1+ST_{b}) - S(1+ST_{b})(1+ST_{b})(1+ST_{b}) - S(1+ST_{b})(1+ST_{b})(1+ST_{b}) - S(1+ST_{b})(1+ST_{b})(1+ST_{b}) - S(1+ST_{b})(1+ST_{b})(1+ST_{b})(1+ST_{b}) - S(1+ST_{b})(1+ST_{b})(1+ST_{b})(1+ST_{b})(1+ST_{b}) - S(1+ST_{b})(1+ST$ $K_p = \begin{subarray}{c} F_{\Delta \geqslant \sigma} & F_{\Delta \geqslant \sigma} & F_{\Delta \implies \sigma} \end{array}$ Kp = D $(e_{10} = 1 = 1 = 0)$ $(+ K_p = \infty) = 0$ Type 1 Samp R(S) = 12 $K_V = U \Delta G(S) H(S)$ $K_{V} = Qt \rightarrow K (1+\delta T_{1})(1+\delta T_{2}) - A$ $\Delta^{20} \rightarrow (1+\delta T_{4})(1+\delta T_{6})$ $K_V = K$ $e_{ss} = I = K_V$ Type I perabolic R(s) = I s^3 $K_{a} = \ell + s^{2} G_{i}(s) H(s) = 0$

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classmate * Type 2 = step R(S) = 1 $A^{2} (1+z_{1}) (1+z_{2}) = \frac{K(1+z_{1})(1+z_{2})}{A^{2}(1+z_{1})(1+z_{2})}$ $K_{ep} = \underset{s \neq 0}{\text{H}} G(s) H(s) = \infty$ $\left(\underset{l+kp}{\text{ess}} = 1 = 0 \right)$ $\begin{array}{c} \not R \\ \hline R(S) = \frac{1}{12} \end{array}$ $K_V = Q t \Delta G(S) H(S) = \infty$ Cos = L = 0 K ۱ ۲ :-* Type 2 parabolic R(S) = 1 2 $K_q = Q + S^2 G_1(S) H(S) = K$ (wr = Un VI-252) resonance feer.

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(p = G(S) = So)(1 + o(S)(S + 10))5) $K\rho = Q + G(S) H(S)$ $\Delta \rightarrow \delta$ = l + 50. $\Delta = 0 (1 + 0.1 \%) (S + 10)$ Kp = 5-> = l + 3 50 = 0 370 (1+0.12) (s+10) = 0 $K_{a} = lt \quad s^{2} \quad So \quad (1 + 0.15)(s + 10)$ $K_q = 0$ -> A Transient response spec. for Second order !-2 3) -> Delay time - It is the time regd. for the casp? to reach So' of the final vo in first time 4. > live time > It is the time regd. to good from to sure gram 10% to 90% of its final val for overdamped & 100 to 100% for an 5. - Reak time 2 go is the time road for the rea to reach the first peak of the time so 6.) or first peak overshoot > Max overshoot > gt is the normalized 6/w the peak of the time xosponse ful 7) -0/P. Max. r. overshoot - C(ts) - (10) (00)

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classmate sottling time - The settling time is the time read for the response to reach and stay within specified range (21. to 5 7. of its final value Palas Plats > Polar plot of sinusoidal r F Gr (jus) is a plot of magn. of G(jue) vis the phase angle of G(jue) on polar coordinates as 'w' varied from 'o' to 'ao' , Hage of Gr(jw) is plotted as the distance from the origin > these angle is measured from the real axis 3 + ve angle measured counter-clockwise 8 - ve angle measured Clackwise > Procedure to skotch the Polar Plat 1) Determine the 7 F G(S) of the system. 2) Put s= jus in transfer fort to obtain Gr (jus) 3) At w=0 & w= 2 . calculate | a(jw) dey lim | G((jw)) & lt | (r (jes)] i) calculate the phase angle of Gr(jiv) at w=0 & w= ~ by lim (Gr (jw) & it (Gr (jes) 2 Rationalize Gr (ju) and separate real and imaginary parts (In 1G (jue))=0), determine freq. at which polar plot intersects the real axis and calculate value -Gr (jus) at this pt. by substituting determined 'us' un Gr(jue)) Re [Gr (jur)] = 0, determine greg. at which polar plat intersects the imaginary axis and calculate the value ef Gr (jus) at this pt by subst detremied to' in G (jus)

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Polar plat for Type 'a' system $G_1(S) = \frac{K}{(1+ST_1)(1+ST_2)}$ 5 = 1 $= \frac{K}{(1+j\omega T_1)(1+j\omega T_2)}$ G(fro) Exite eq. a. in polar form tan-wTi-ten wi Jehan ary 1 1/w the Jol+ (0 T2)2 U=0 lt Grijus = K $U = \infty$ lt |G(y|u)| = K = 0Phase w=0 lt -turioT, - tan'wTz = 0 W--∞ lt -tai wT1 - tai wT2 = -180° w> 2200

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classmate Date Equate seal part $\tau_0 = 0$ $K(1 - \omega^2 T_1 T_2) = 0$ w = 1 $\sqrt{\tau_1 \tau_2}$ (freq. at which polar " flat intersect imag. cixis $G_1(jw)$ at w = 1 $\sqrt{T_1, T_2}$ $K\left(1-\frac{T_{1}T_{2}}{T_{1}T_{2}}\right) - \frac{jK\left(\frac{T_{1}+T_{2}}{\sqrt{T_{1}T_{2}}}\right)}{\sqrt{T_{1}T_{2}}}$ Ø $1 + \frac{1}{12} + \frac{1}{112} + \frac{1}{112} + \frac{1}{112} + \frac{1}{12} + \frac{$ = - JR JTITZ $T_1 + T_2$ 1 Gr(jur) = K JT, TL T,+T2 ange at w = 1/JTITZ $\phi = \tan^{-1} \left(\frac{-k\omega \left(T_{1} + T_{2} \right)}{k \left(1 - \omega^{2} T_{1} \tau_{2} \right)} \right)$ $\oint = -90^{\circ}$ 220 Im Ky V =0 08 Re -185 <u>kJT, T2</u> T, + T2 UT.TZ -90 Polar plat for standard fits G(S) = VSii) 6 = 1/52 iii) Gr(1/= +, Ting 15=0 > Re W=a 5-0 5=00 5=0 Tw inc >Re 2 W=20

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