

# Control System

Intro  $\rightarrow$  Behaviour of the system is described by differential eq<sup>n</sup>. 2 types :-

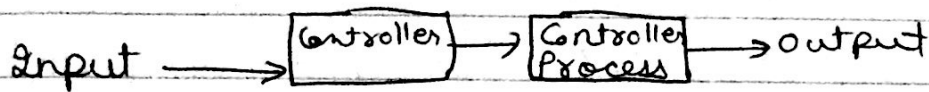
i) open loop C.S

ii) closed loop C.S

open loop  $\rightarrow$   $\rightarrow$  No feedback.

$\rightarrow$  independent of desired o/p.

$\rightarrow$  o/p not compared with ref. i/p.



## Advantages

simple

economical

less maintenance

Proper calibration is not a problem

## Disadvantages

i) Inaccurate

ii) Not reliable

iii) slow

iv) Optimization is not possible.

$\rightarrow$  immersion rod for water heating.  
 $\rightarrow$  automatic washing machine.

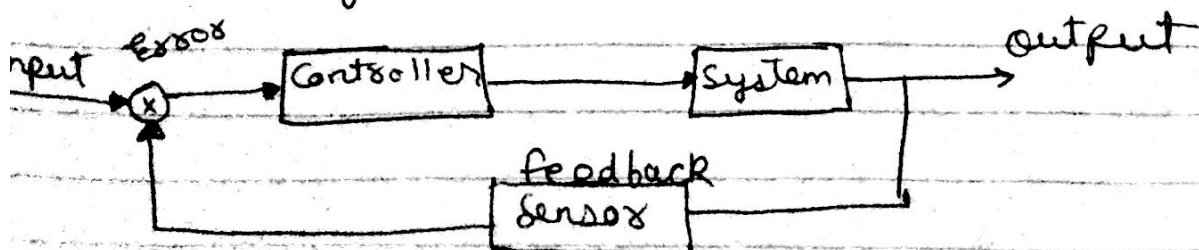
## Closed Loop system

feedback

dependent on desired o/p.

one or more feedback possible.

Error signal produce.





- Adv.
- more reliable
  - faster
  - optimization is possible

- Disadv.
- Expensive
  - Diff. maintenance
  - complicated installation

E.g. → A.C (Thermostat)

### Comparison

#### Open loop

- i) Perform accurately if the calibration is good.
- ii) Easier to build.
- iii) More stable
- iv) Optimization not possible
- v) Economical

#### Closed Loop

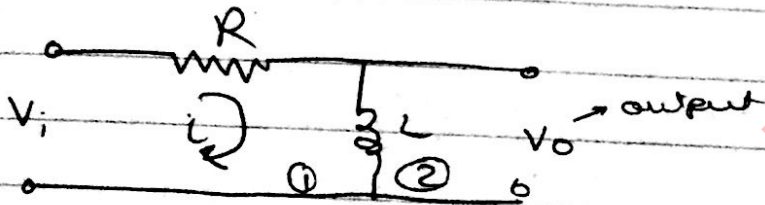
- i) Perform better than of the feedback.
- ii) Diff. to build. becos of feedback
- iii) Less stable than open loop.
- iv) Optimization is possible.
- v) Expensive.



Transfer fnt.  $\rightarrow$  ratio of Laplace transform of the o/p to the Laplace transform of i/p, with all initial condition 0.

$$T.F / G(s) = \frac{C(s)}{R(s)}$$

find  $G(s)$



apply KVL

$$V_i = Ri + L \frac{di}{dt}$$

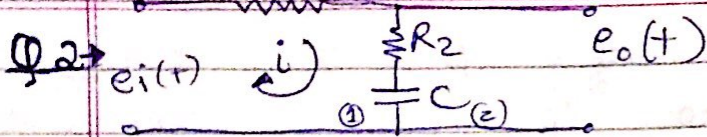
$$V_i(s) = Ri(s) + sLi(s)$$

apply KVL in mesh

$$V_o = L \frac{di}{dt}$$

$$V_o(s) = sLi(s)$$

$$G(s) = \frac{V_o(s)}{V_i(s)} = \frac{sLi(s)}{Ri(s) + sLi(s)}$$



$$\textcircled{1} \quad e_i(t) = R_1 i(t) + R_2 i(t) + \frac{1}{C} \int i(t) dt$$

$$E_i(s) = I(s) \left[ R_1 + R_2 + \frac{1}{Cs} \right]$$

$$\textcircled{2} \quad e_o(t) = R_2 i(t) + \frac{1}{C} \int i(t) dt$$

$$E_o(s) = I(s) \left[ R_2 + \frac{1}{Cs} \right]$$

$$\text{T.F.} = \frac{E_o(s)}{E_i(s)} = \frac{I(s) \left[ R_2 + \frac{1}{Cs} \right]}{I(s) \left[ R_1 + R_2 + \frac{1}{Cs} \right]}$$

~~$$= \frac{R_2 + \frac{1}{Cs}}{R_1 + R_2 + \frac{1}{Cs}}$$~~

$$= \frac{1 + R_2 Cs}{1 + (R_1 + R_2) Cs}$$

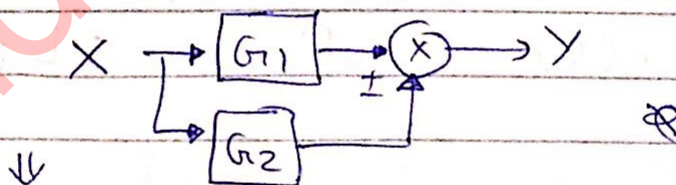
★ Block diagram reduction.

i) Combining blocks in Cascade/series.

$$X \rightarrow [G_1] \rightarrow [G_2] \rightarrow Y \quad \Rightarrow \quad X \rightarrow [G_1 \cdot G_2] \rightarrow Y$$

$$Y = (G_1 G_2) X$$

ii) Combining blocks in Parallel

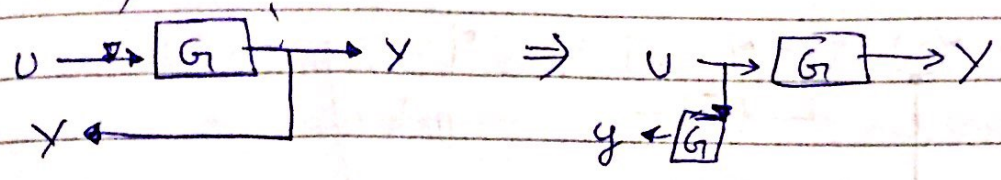


$$X \rightarrow [G_1 \pm G_2] \rightarrow Y$$

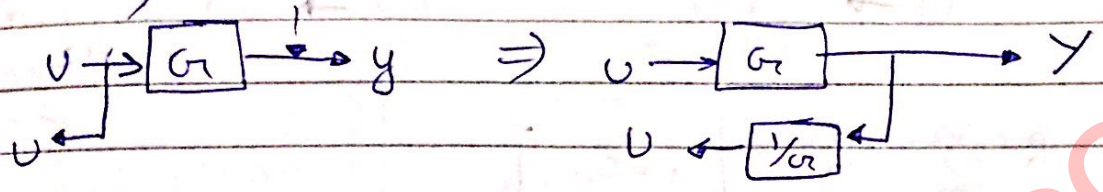
$$Y = (G_1 \pm G_2) X$$



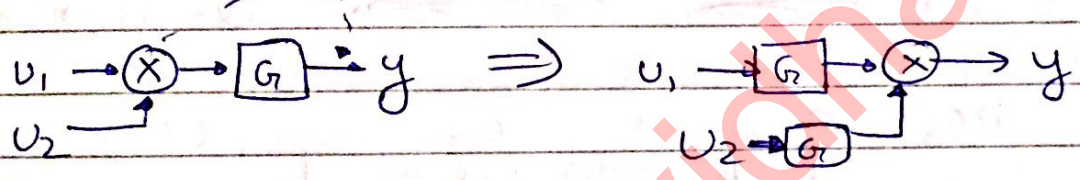
3) Moving a pickoff point ~~before~~ a block



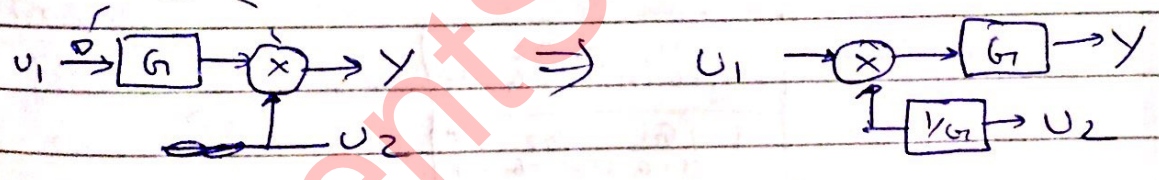
4) Moving a pickoff point behind a block



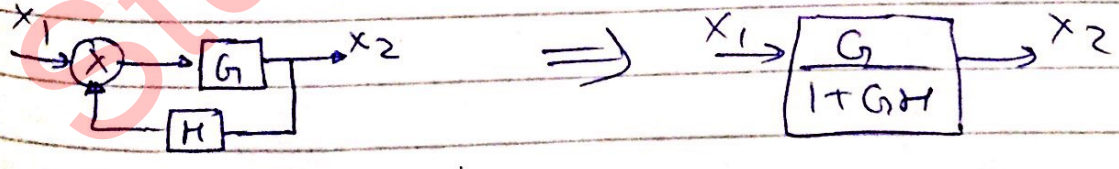
5) Moving a summing pt. behind a block



6) Moving a summing pt. ahead of a block

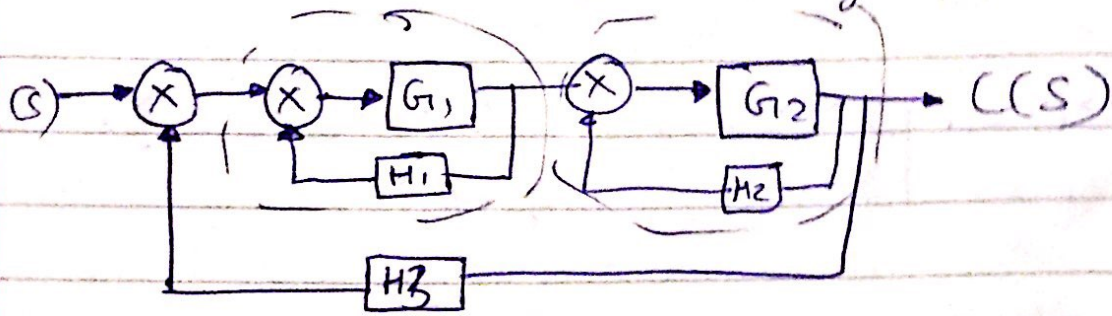


7) Eliminating feedback path





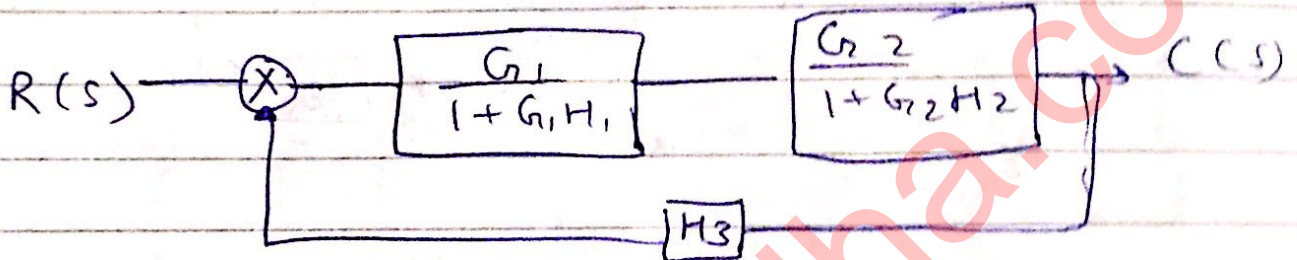
Reduce the block diagram



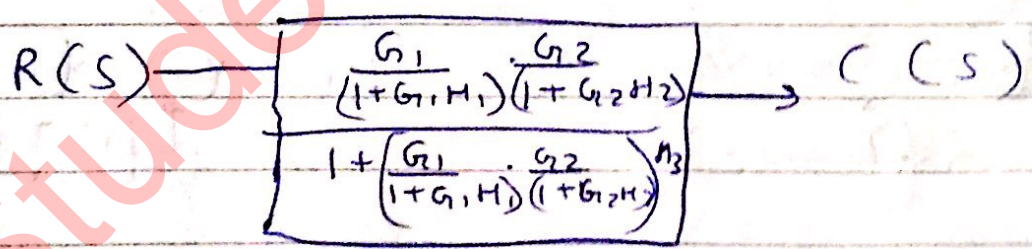
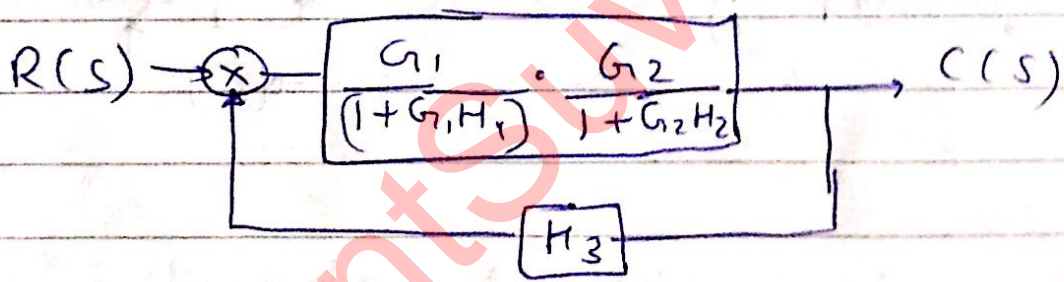
eliminating feedback paths

①  $\rightarrow \frac{G_1}{1 + G_1 H_1}$

②  $\rightarrow \frac{G_2}{1 + G_2 H_2}$



~~Rule (1)~~ Rule (1)  $\rightarrow$





## → Signal Flow Graph

- Developed by S. J. Mason for Block diagram reduction of complicated systems.
- In signal flow graph, each node  $\Rightarrow$  system variable. Each branch connected b/w 2 nodes  $\Rightarrow$  signal multiplier. Direction of signal flow  $\Rightarrow$  arrow.

## \* Terminologies

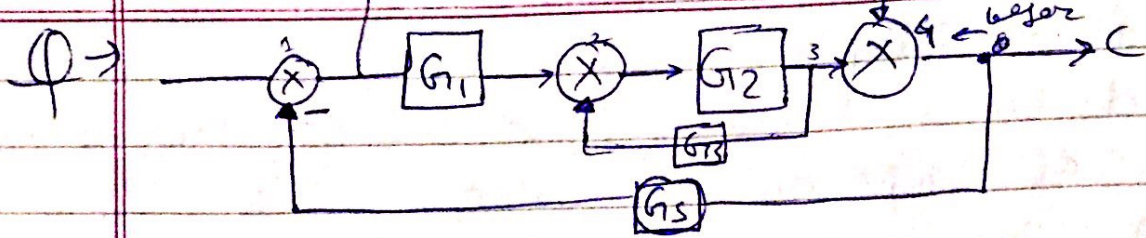
- Node  $\rightarrow$  variable
- Loop  $\rightarrow$  closed path
- Loop Gain  $\rightarrow$  Product of branch ~~transmittance~~ <sup>Transfer fct</sup> <sub>b/w 2 nodes</sub> ~~attenuances~~ of loop.
- Non-touching loop  $\rightarrow$  No common node
- f/w path  $\rightarrow$  Path from i/p to o/p node which does not cross any node more than once.
- f/w path Gain  $\rightarrow$  Product of branch transmittance of a fwd. path.

## \* Mason's Gain formula

$$T = \sum_K \frac{P_K \Delta_K}{\Delta} \quad \text{where } P_K \rightarrow \text{Path Gain of fwd path}$$

$$\Delta = 1 - \left[ \text{Sum of all individual loop gain} \right] + \left[ \text{Sum of all possible loop gain of 2 non-touching loops} \right] - \left[ \text{Sum of all possible gain products of 3 non-touching loops} \right] + \dots$$

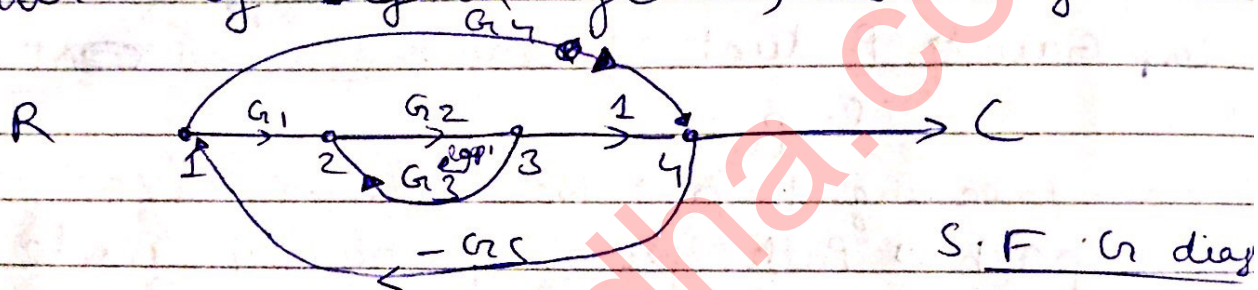




Rules for B.D to S.F G

→ Represent all variables (summing pt, takeoff pt) by nodes

→ If summing pt is before take off pt. in dir<sup>n</sup> of signal flow, use single node



Mason Gain's formula

$$T_K = \frac{\sum G_K \Delta_K}{\Delta}$$

i) f/w paths =  $P_1 (1, 2, 3, 4) = \text{gain } G_1 (G_2, G_3)$   
 $= P_2 (1, 4) = G_4 (G_5)$

ii) find individual loop gain

$$L_1 (2, 3) = \text{gain} = G_2 G_3$$

$$L_2 (1, 4, 1) \quad \text{gain} = (-G_4 G_5)$$

$$L_3 (1, 2, 3, 4) \quad \left[ \text{gain} = -G_1 G_2 G_3 G_5 \right]$$



find all 2 not touching loops

$L_1$  &  $L_2$  are not touching

$$L_1 L_2 \text{ (gain} = -G_2 G_3 G_4 G_5)$$

calculate  $\Delta$ ,

$$\Delta = 1 - \left[ \text{sum of individual loop gain} \right] + \left[ \text{sum of all } \cancel{\text{2}} \text{ not touching} \right]$$

$$\Delta = 1 - \left[ G_2 G_3 - G_4 G_5 - G_1 G_2 G_5 \right] + \left[ -G_2 G_3 G_4 \right]$$

$$\Delta = 1 - G_2 G_3 + G_4 G_5 + G_1 G_2 G_5 - G_2 G_3 G_4 G_5$$

Calculate  $\Delta_k$

$\Delta_1 =$  Part of  $\Delta$  not touching Path 1 ( $P_1$ )

$$\Delta_1 = 1$$

$\Delta_2 =$  Part of  $\Delta$  not touching Path 2 ( $P_2$ )

$$\Delta_2 = 1 - G_2 G_3$$

$$T = \frac{\sum \Delta_k P_k}{\Delta} = \frac{\Delta_1 g_1 + \Delta_2 g_2}{\Delta}$$

$$= \frac{1(G_1 G_2) + (1 - G_2 G_3) G_1}{\Delta}$$