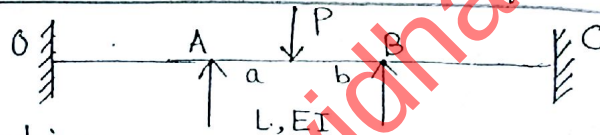


Slope Deflection Method

- Given by G.A. Maney.
- Based on stiffness concept.
- Suitable when $D_k < D_s$
- Basic unknowns are taken joint displacements (or).
- To find joint displacements, joint equilibrium & shear equations are written.
- To find moment in members - force displacement relations are written called slope deflection equations
- Axial deformations are neglected but shear displacements are considered.

Derivation of slope-deflection equation-



sign convention-

1. To compute end moments.



2. Slope



3. Deflection

Those displacement taken '+ve' which will produce clockwise rotation to the member and hence '+ve' displacement will produce '-ve' moments.

Step 1 → Consider span AB → The effect of loading present

$$\bar{M}_{AB} = -\frac{Pab^2}{L^2} \quad (\text{fixed end moment at A in span AB})$$

$$\bar{M}_{BA} = \frac{Pa^2b}{L^2} \quad (\text{fixed end moment at B in span A})$$

Step 2 → If joint A rotates by angle θ_A , then F.E.M. developed at A in AB

$$= \frac{4EI}{L} \theta_A$$

and carry over moment at B due to θ_A
$$= \frac{2EI}{L} \cdot \theta_A$$

step 3 $\rightarrow$ Effect of θ_B

If joint B rotates by θ_B , then moment developed at B = $\frac{4EI}{L} \cdot \theta_B$

and carry over moment at A = $\frac{2EI}{L} \cdot \theta_B$

step 4 $\rightarrow$ If support B settles down with respect to support A by Δ which causes rotation of AB in clockwise direction, then F.E.M. produce at A and B will be, $-\frac{6EI}{L^2} \Delta$ at A & $-\frac{6EI}{L^2} \Delta$ at B.

The final moment at end A and B due to above multiple effect will be,

$$M_{AB} = \bar{M}_{AB} + \frac{4EI}{L} \theta_A + \frac{2EI}{L} \theta_B - \frac{6EI}{L^2} \Delta$$

$$M_{AB} = \bar{M}_{AB} + \frac{2EI}{L} \left(2\theta_A + \theta_B - \frac{3\Delta}{L} \right)$$

Slope deflection equation at A for AB.

OR
force displacement Relation

slope deflection equation at B,

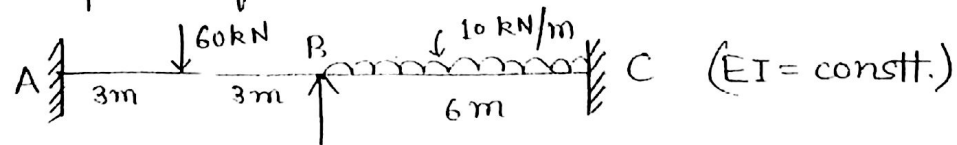
$$M_{BA} = \bar{M}_{BA} + \frac{2EI}{L} \left(2\theta_B + \theta_A - \frac{3\Delta}{L} \right)$$

step 5 $\rightarrow$ To find joint displacements (θ & Δ), moment equilibrium conditions at joints and shear equations are written.

No. of moment equi. conditions = No. of rotational displacement

No. of shear eqns = No. of linear displacement component.

Example - Analyse the beam shown in figure using slope deflection method.



$$\bar{M}_{AB} = -\frac{PL}{8} = -45$$

$$\bar{M}_{BA} = +45$$

$$\bar{M}_{BC} = -\frac{wl^2}{12} = -30$$

$$\bar{M}_{CB} = +30$$

$$M_{AB} = \bar{M}_{AB} + \frac{2EI}{L} \left(2\theta_A + \theta_B - \frac{3\Delta}{L} \right)$$

$$M_{AB} = -45 + \frac{EI}{3} \theta_B \quad (1)$$

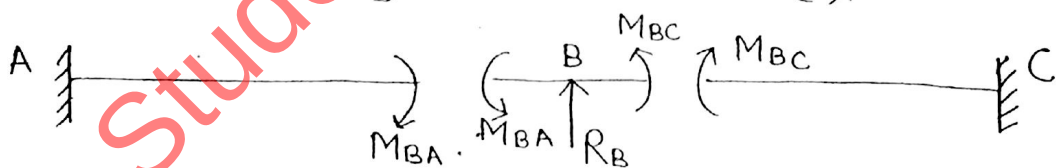
$$M_{BA} = +45 + \frac{2EI}{L} \left(2\theta_B + \theta_A - \frac{3\Delta}{L} \right)$$

$$M_{BA} = +45 + \frac{EI}{3} (2\theta_B) \quad (2)$$

$$M_{BC} = -30 + \frac{2EI}{L} \left(2\theta_B + \theta_C - \frac{3\Delta}{L} \right)$$

$$M_{BC} = -30 + \frac{EI}{3} (2\theta_B) \quad (3)$$

$$M_{CB} = +30 + \frac{EI}{3} \theta_B \quad (4)$$



Joint equilibrium equation at B,

$$\sum M_B = 0$$

$$M_{BA} + M_{BC} = 0$$

$$45 + \frac{EI}{3} (2\theta_B) + (-30) + \frac{EI}{3} (2\theta_B) = 0$$

$$\frac{EI}{3} \times 4\theta_B = -15$$

$$\theta_B = -\frac{11.25}{EI} \quad \text{C}$$

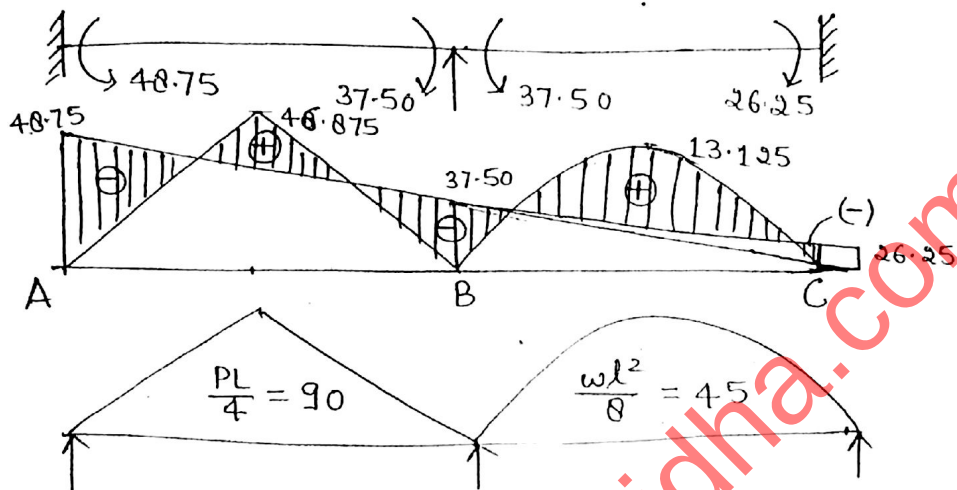
From equation (1), (2), (3) and (4).

$$M_{AB} = -45 - \frac{11.25}{3} = -48.75$$

$$M_{BA} = 45 - \frac{2}{3} \times 11.25 = +37.50$$

$$M_{BC} = -37.50$$

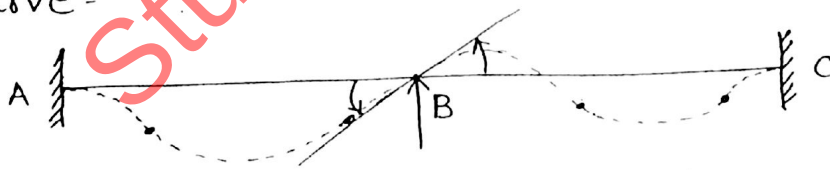
$$M_{CB} = 30 - \frac{11.25}{3} = +26.25$$



$$\text{Net BM at centre of AB} = 90 - \left(\frac{48.75 + 37.50}{2} \right) = 46.875 \text{ kN-m}$$

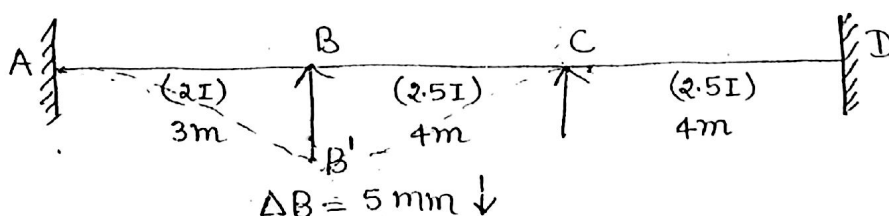
$$\text{Net BM at centre of BC} = 45 - \left(\frac{37.50 + 26.25}{2} \right) = 13.125 \text{ kN-m}$$

Elastic Curve -



Question - Analyse the continuous beam shown in figure by slope deflection method if support B settles down by 5 mm. Given that $E = 2 \times 10^5 \text{ N/mm}^2$ and

$$I = 36 \times 10^6 \text{ mm}^4$$



$$M_{AB} = \bar{M}_{AB} + \frac{2EI}{L} \left(2\theta_A + \theta_B - \frac{3\Delta}{L} \right)$$

$$= 0 + \frac{2E(2I)}{L} \left(0 + \theta_B - 3 \times \frac{5 \times 10^{-3}}{3} \right)$$

$$M_{AB} = \frac{4EI}{3} (\theta_B - 5 \times 10^{-3}) \quad \text{--- (1)}$$

$$M_{BA} = \frac{4EI}{3} (2\theta_B - 5 \times 10^{-3}) \quad \text{--- (2)}$$

$$M_{BC} = 0 + \frac{2E}{4} (2.5I) \left(2\theta_B + \theta_C + \frac{3 \times 5 \times 10^{-3}}{4} \right)$$

$$M_{BC} = \frac{5}{4} EI (2\theta_B + \theta_C + \frac{15}{4} \times 10^{-3}) \quad \text{--- (3)}$$

$$M_{CB} = \frac{5}{4} EI (2\theta_C + \theta_B + \frac{15}{4} \times 10^{-3}) \quad \text{--- (4)}$$

$$M_{CD} = \frac{2E(2.5I)}{4} \left(2\theta_C + \theta_D - \frac{3\Delta}{L} \right)$$

$$M_{CD} = \frac{5}{4} EI (2\theta_C) \quad \text{--- (5)}$$

$$M_{DC} = \frac{5}{4} EI (\theta_C) \quad \text{--- (6)}$$

Joint equations,

$$\sum M_B = 0,$$

$$M_{BA} + M_{BC} = 0$$

$$\frac{4EI}{3} (2\theta_B - 5 \times 10^{-3}) + \frac{5}{4} EI (2\theta_B + \theta_C + \frac{15}{4} \times 10^{-3}) = 0$$

$$16(2\theta_B - 5 \times 10^{-3}) + 15(2\theta_B + \theta_C + \frac{15}{4} \times 10^{-3}) = 0$$

$$62\theta_B + 15\theta_C - 23.75 \times 10^{-3} = 0 \quad \text{--- (A)}$$

$$\sum M_C = 0,$$

$$M_{CB} + M_{CD} = 0$$

$$\frac{5}{4} EI (2\theta_C + \theta_B + \frac{15}{4} \times 10^{-3}) + \frac{5}{4} EI (2\theta_C) = 0$$

$$4\theta_C + \theta_B + 3.75 \times 10^{-3} = 0 \quad \text{--- (B)}$$

$$\text{eqn (A)} \times 4 - \text{eqn (B)} \times 15,$$

$$(62 \times 4 - 15) \theta_B - (23.75 \times 4 + 3.75 \times 15) \times 10^{-3} = 0$$

$$\boxed{\theta_B = 6.49 \times 10^{-4}}$$

from eqns (B),

$$4\theta_C = -4.399 \times 10^{-3}$$

$$\boxed{\theta_C = -1.10 \times 10^{-3}}$$

Final moments,

$$M_{AB} = -41.77$$

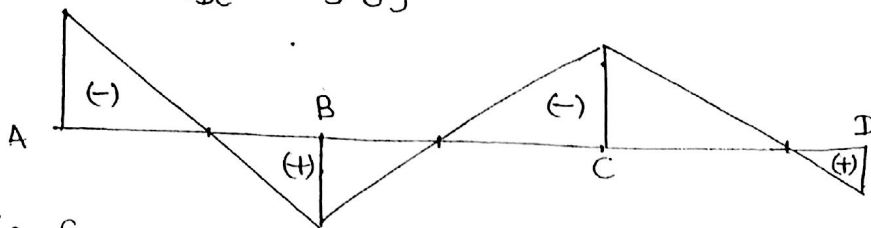
$$M_{BA} = -35.53$$

$$M_{BC} = +35.53$$

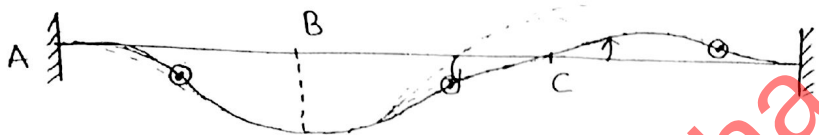
$$M_{CD} = -19.78$$

$$M_{DC} = -9.89$$

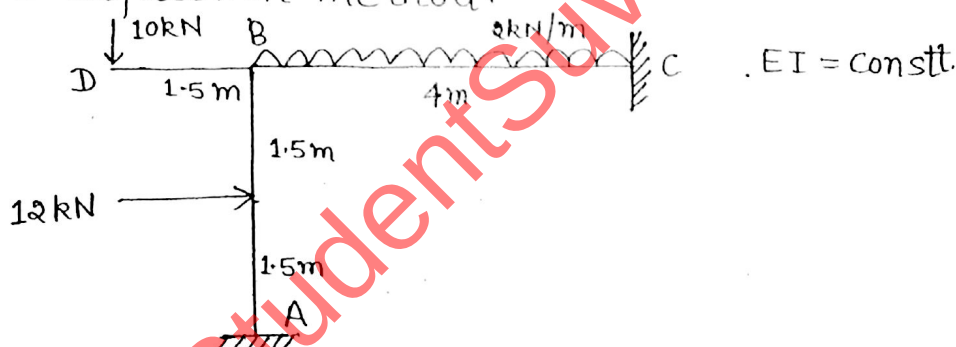
BMD



Elastic Curve,



Question- Analyse the frame shown in figure by slope deflection method.



Fixed end Moments,

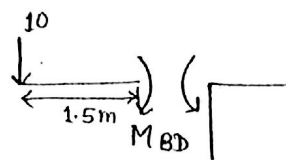
$$\bar{M}_{AB} = -\frac{12 \times 3}{8} = -4.5$$

$$\bar{M}_{BA} = +4.5$$

$$\bar{M}_{BC} = -32$$

$$\bar{M}_{CB} = +32$$

$$\bar{M}_{BD} = 15 \text{ kN-m}$$



$$\therefore M_{AB} = -4.5 + \frac{2EI}{3} \left(2\theta_A + \theta_B - \frac{3\Delta}{L} \right)$$

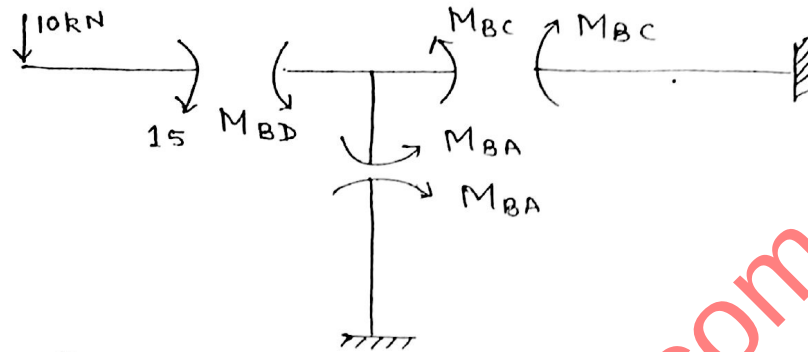
$$M_{AB} = -4.5 + \frac{2EI}{3} \cdot \theta_B \quad \text{--- (1)}$$

$$M_{BA} = +4.5 + \frac{2EI}{3} (2\theta_B) \quad \text{--- (2)}$$

$$M_{BC} = -32 + \frac{2EI}{4} (2\theta_B + \theta_C - \frac{3\Delta}{L})$$

$$M_{BC} = -32 + \frac{2EI}{4} (2\theta_B) \quad \text{--- (3)}$$

$$M_{CB} = +32 + \frac{EI}{2} \theta_B \quad \text{--- (4)}$$



$$\sum M_B = 0,$$

$$-15 - M_{BA} - M_{BC} = 0$$

$$+15 + 4.5 + \frac{2EI}{3} \times 2\theta_B + (-32) + EI\theta_B = 0$$

$$(\frac{4}{3}\theta_B + \theta_B)EI = 12.5$$

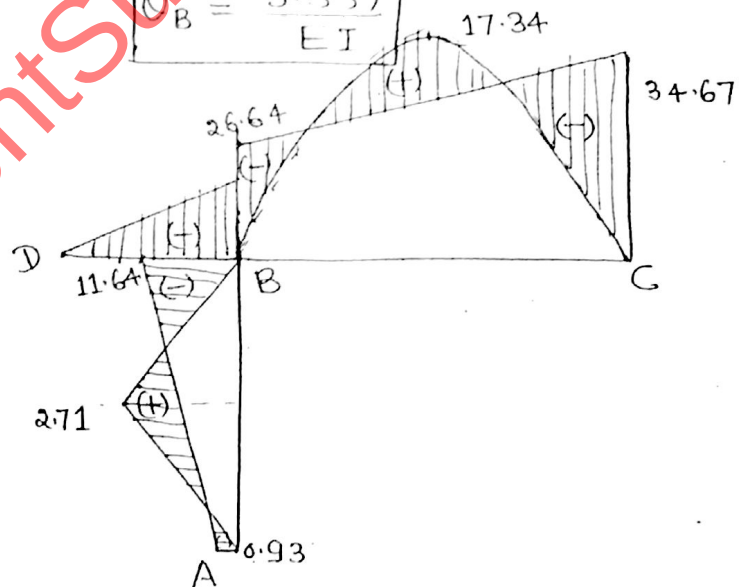
$$\theta_B = \frac{5.357}{EI}$$

$$M_{AB} = -0.93$$

$$M_{BA} = +11.64$$

$$M_{BC} = -26.64$$

$$M_{CB} = +34.67$$

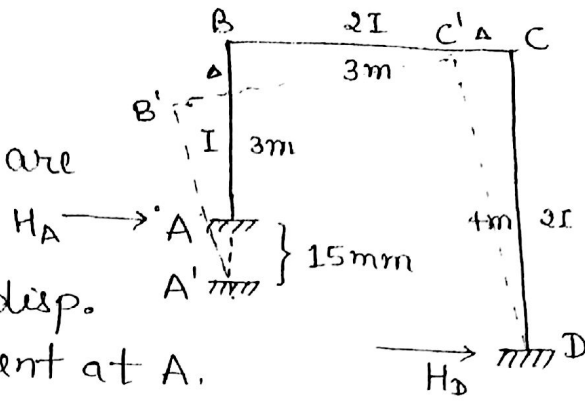


Question For the frame shown in figure, support A settles by 15 mm vertically down. Analyse the frame by slope deflection method and draw BMD. $EI = 48000 \text{ kN-m}^2$. Draw deflected shape of the frame.

$$\Delta = 15 \text{ mm} \downarrow$$

Horizontal component of displacement at B and C are equal = Δ

vertical component of disp. at B = Vertical displacement at A.



$$M_{AB} = \bar{M}_{AB} + \frac{2EI}{3} (2\theta_A + \theta_B + \frac{3\Delta}{3})$$

$$M_{AB} = \frac{2EI}{3} (\theta_B + \Delta) \quad \text{--- (1)}$$

$$M_{BA} = \frac{2EI}{3} (2\theta_B + \Delta) \quad \text{--- (2)}$$

$$M_{BC} = 0 + \frac{2E}{3} (2I) (2\theta_B + \theta_C + \frac{3 \times 15 \times 10^{-3}}{3})$$

$$M_{BC} = \frac{4EI}{3} (2\theta_B + \theta_C + 15 \times 10^{-3}) \quad \text{--- (3)}$$

$$M_{CB} = \frac{4EI}{3} (2\theta_C + \theta_B + 15 \times 10^{-3}) \quad \text{--- (4)}$$

$$M_{CD} = 0 + \frac{2E}{4} (2I) (2\theta_C + \theta_D + \frac{3}{4} \Delta)$$

$$M_{CD} = EI (\theta_C + \frac{3}{4} \Delta) \quad \text{--- (5)}$$

$$M_{DC} = EI (\theta_C + \frac{3}{4} \Delta) \quad \text{--- (6)}$$

$$\sum M_B = 0,$$

$$M_{BA} + M_{BC} = 0 \quad \text{--- (A)}$$

$$\sum M_C = 0,$$

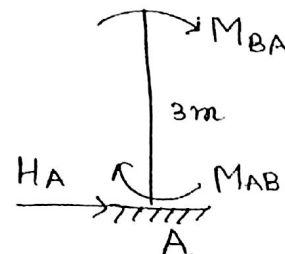
$$M_{CB} + M_{CD} = 0 \quad \text{--- (B)}$$

Shear equation,

$$\sum F_x = 0, \quad H_A + H_D = 0$$

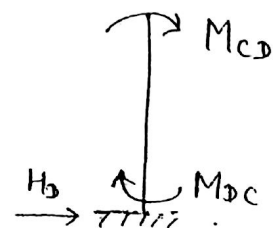
$$-H_A \times 3 + M_{AB} + M_{BA} = 0$$

$$H_A = \frac{M_{AB} + M_{BA}}{3} \quad \text{--- (C)}$$



$$-H_D \times 4 + M_{CD} + M_{DC} = 0$$

$$H_D = \left(\frac{M_{DC} + M_{CD}}{4} \right) \quad \text{--- (D)}$$



$$\therefore \left(\frac{M_{AB} + M_{BA}}{3} \right) + \left(\frac{M_{DC} + M_{CD}}{4} \right) = 0 \quad \text{--- (E)}$$

From joint equations and shear equations θ_B , θ_C , Δ are obtained and final values of moment are found as,

$$M_{AB} = +91.63$$

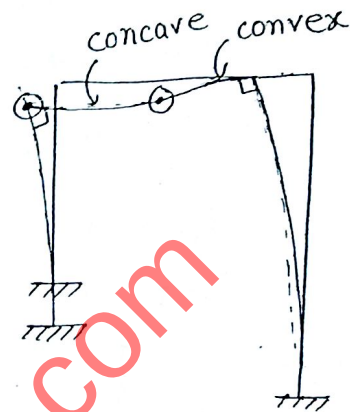
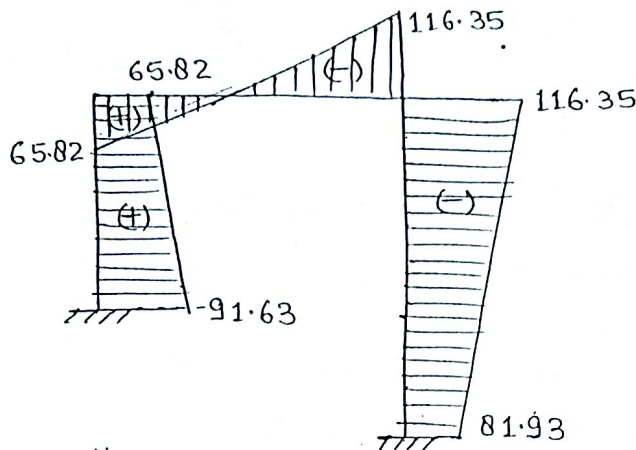
$$M_{CB} = +116.35$$

$$M_{BA} = -65.82$$

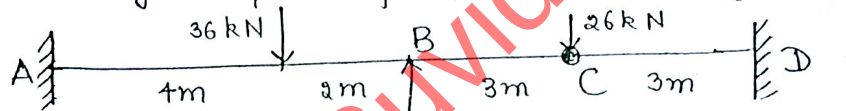
$$M_{CD} = -116.35$$

$$M_{BC} = +65.82$$

$$M_{DC} = +81.93$$



Question For the Beam shown in figure, Draw BMD using slope deflection method.



θ_B , θ_C , θ_{C_2} (Just to right of C), Δ_C = unknown.

$D_k = 3\bar{f} - r_e + r_s$ - Axial deformation

$$D_k = 3 \times 4 - 7 + 1 - 2 \quad \begin{matrix} \rightarrow \text{at B} \\ \rightarrow \text{at C} \end{matrix}$$

$$D_k = 4$$

$$\bar{M}_{AB} = -16, \quad \bar{M}_{BA} = 32$$

$$\bar{M}_{BC} = \bar{M}_{CB} = 0$$

$$\bar{M}_{CD} = \bar{M}_{DC} = 0$$

$$M_{AB} = -16 + \frac{2EI}{6} (2\theta_A + \theta_B - \frac{3\Delta}{6})$$

$$M_{AB} = -16 + \frac{EI}{3} \theta_B \quad \text{--- (1)}$$

$$M_{BA} = +32 + \frac{EI}{3} (2\theta_B) \quad \text{--- (2)}$$

$$M_{BC} = 0 + \frac{2EI}{3} (2\theta_B + \theta_{C1} - \frac{3\Delta_C}{3})$$

$$M_{BC} = \frac{2EI}{3} (2\theta_B + \theta_{C1} - \Delta_C) \quad \text{--- (2)}$$

$$M_{CB} = \frac{2EI}{3} (\theta_B + 2\theta_{C1} - \Delta_C) \quad \text{--- (4)}$$

$$M_{CD} = 0 + \frac{2EI}{3} (2\theta_{C2} + \theta_B + \frac{3\Delta_C}{3}) \quad \text{--- (5)}$$

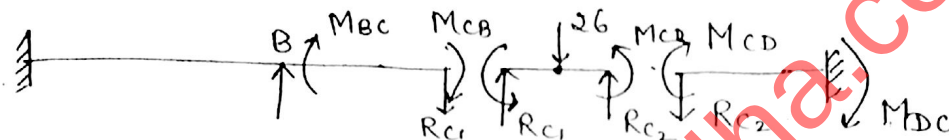
$$M_{DC} = \frac{2EI}{3} (\theta_{C2} + \Delta_C) \quad \text{--- (6)}$$

Joint conditions,

$$\Sigma M_B = 0, \quad M_{BA} + M_{BC} = 0 \quad \text{--- (A)}$$

$$M_{CB} = 0 \quad \text{--- (B)}$$

$$M_{CD} = 0 \quad \text{--- (C)}$$



Shear equation at C,

$$\Sigma F_y = 0, \quad R_{C1} + R_{C2} - 26 = 0$$

To find R_{C1} pick moment just to right of B.

$$R_{C1} \times 3 + M_{BC} + M_{CB} = 0$$

$$R_{C1} = -\frac{M_{BC}}{3}$$

To find R_{C2} take moment about D,

$$M_{CD} + M_{DC} - R_{C2} \times 3 = 0$$

$$M_{DC} - R_{C2} \times 3 = 0$$

$$R_{C2} = \frac{M_{DC}}{3}$$

Shear equation,

$$-\frac{M_{BC}}{3} + \frac{M_{DC}}{3} = 26$$

$$M_{DC} - M_{BC} = 78 \quad \text{--- (D)}$$

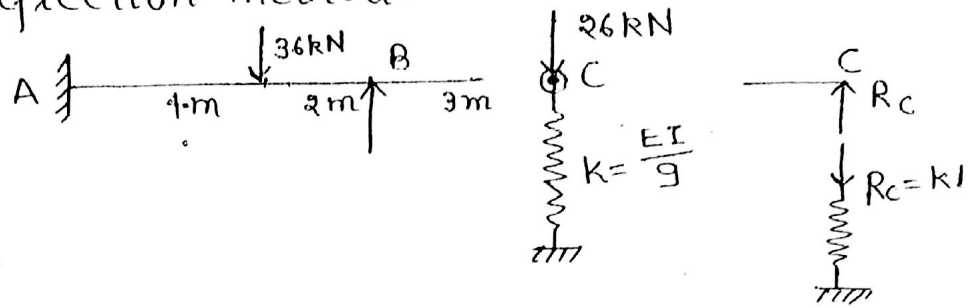
solving eqns (A), (B), (C) and (D), final moments;

$$M_{AB} = -14 \text{ kN-m} \quad M_{CB} = 0$$

$$M_{BA} = +36 \text{ kN-m} \quad M_{CD} = 0$$

$$M_{BC} = -36 \text{ kN-m} \quad M_{DC} = +42 \text{ kN-m}$$

Question - Analyse the beam section shown in figure by slope deflection method.



$$\bar{M}_{AB} = -16$$

$$\bar{M}_{BA} = +32$$

$$\bar{M}_{BC} = \bar{M}_{CB} = 0$$

$$M_{AB} = -16 + \frac{2EI}{6} (2\theta_A + \theta_B - \frac{3\Delta_A}{L})$$

$$M_{AB} = -16 + \frac{EI}{3} \theta_B \quad \text{--- (1)}$$

$$M_{BA} = +32 + \frac{EI}{3} \cdot 2\theta_B \quad \text{--- (2)}$$

$$M_{BC} = 0 + \frac{2EI}{3} [2\theta_B + \theta_C - \frac{3\Delta_C}{3}]$$

$$M_{BC} = \frac{2EI}{3} (2\theta_B + \theta_C - \Delta_C) \quad \text{--- (3)}$$

$$M_{CB} = \frac{2EI}{3} (2\theta_C + \theta_B - \Delta_C) \quad \text{--- (4)}$$

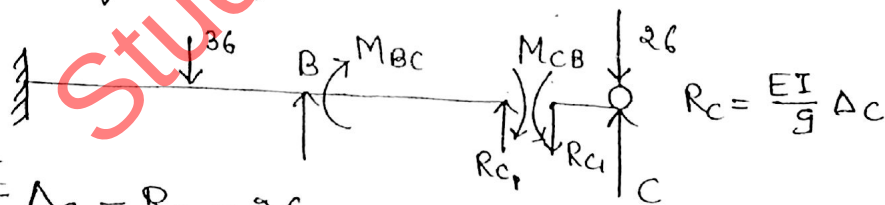
Joint equations at B,

$$M_{BA} + M_{BC} = 0 \quad \text{--- (A)}$$

Joint equations at C,

$$M_{CB} = 0 \quad \text{--- (B)}$$

Shear equation,



$$\frac{EI}{9} \Delta_C - R_{C1} - 26 = 0$$

R_{C1} can be found by taking moment just to the right of B,

$$-R_{C1} \times 3 + M_{BC} = 0 \quad (\because M_{CB} = 0)$$

Hence, shear equation is,

$$\frac{EI}{9} \Delta_C - \frac{M_{BC}}{3} - 26 = 0 \quad \text{--- (C)}$$

From equations (A), (B) and (C),
 θ_A , θ_B and Δ_c are known and final moments are

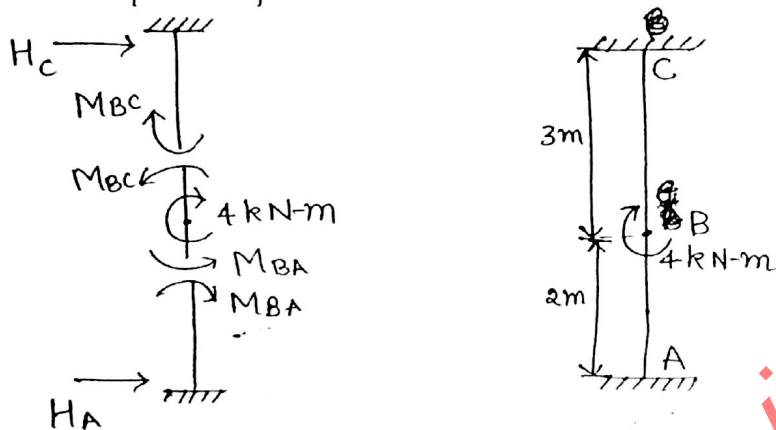
$$M_{AB} = -14 \text{ kN-m}$$

$$M_{BA} = +36 \text{ kN-m}$$

$$M_{BC} = -36 \text{ kN-m}$$

$$M_{CB} = 0$$

Question Analyse the frame shown in figure using slope deflection method-



For joint B,

$$\sum M = 0$$

$$-M_{BA} - M_{BC} + 4 = 0$$

$$M_{BA} + M_{BC} = 4 \quad \text{--- (1)}$$

Shear equation,

$$H_A + H_C = 0$$